

**ECE ECE145A (undergrad) and ECE218A (graduate)  
Final Exam. Monday December 5, 2021, noon - 3 p.m.**

Open book. You have 3 hrs.

Use all reasonable approximations (5% accuracy is fine. ),

***AFTER STATING and justifying THEM.***

***Think before doing complex calculations. Sometimes there is an easier way.***

Problem	Points Received	Points Possible
1A		5
1B		5
1C		5
1D		5
1D		5
1F		10
1G		10 (218A only)
2		10
3		10
4A		10
4B		10 (218A only)
5A		5
5B		10 (218A only)
total		70 (145A), 100 (218A)

$$G_T = \frac{|S_{21}|^2 (1 - |\Gamma_s|^2)(1 - |\Gamma_L|^2)}{|(1 - \Gamma_s S_{11})(1 - \Gamma_L S_{22}) - S_{21} S_{12} \Gamma_s \Gamma_L|^2} \quad G_P = \frac{1}{1 - \|\Gamma_{in}\|^2} \cdot |S_{21}|^2 \cdot \frac{1 - |\Gamma_L|^2}{|1 - \Gamma_L S_{22}|^2}$$

$$G_a = \frac{1 - |\Gamma_s|^2}{|1 - \Gamma_s S_{11}|^2} \cdot |S_{21}|^2 \cdot \frac{1}{1 - \|\Gamma_{out}\|^2} \quad G_{max} = \frac{|S_{21}|}{|S_{12}|} \cdot \left[ K - \sqrt{K^2 - 1} \right] \text{ if } K > 1$$

$$G_{MS} = \frac{|S_{21}|}{|S_{12}|} \cdot \text{if } K < 1 \quad K = \frac{1 - |S_{11}|^2 - |S_{22}|^2 + |\Delta|^2}{2 |S_{21} S_{12}|} \quad \text{where } \Delta = \det[S]$$

Unconditionally stable if : (1)  $K > 1$  **and** (2)  $\|\det[S]\| < 1$

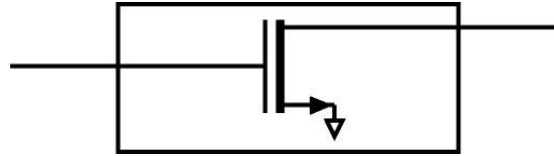
**Problem 1, 30 points (145A), 40 points (218A)**

*Power Gain Definitions*

part a, 5 points

At 100 GHz, the transistor has  
 $S_{11} = -1/2$ ,  $S_{21} = -4$ ,  $S_{12} = 0$ ,  $S_{22} = +1/3$ ,  
(S-parameters using  $50\Omega$  normalization)

The generator has  $(250/3)$  Ohms source impedance and 1 mW available power. The load is  $(50/3)$  Ohms.



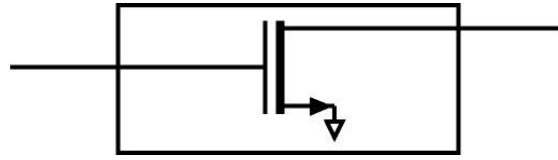
If we directly connect the generator to the transistor input, but impedance-match the load to the transistor output, what RF power will be delivered to the load ?

RF power delivered to the load = \_\_\_\_\_

part b. 5 points

At 100 GHz, the transistor has  
 $S_{11} = -1/2$ ,  $S_{21} = -4$ ,  $S_{12} = 0$ ,  $S_{22} = +1/3$ ,  
(S-parameters using  $50\Omega$  normalization)

The generator has 50 Ohms source impedance and 1 mW available power. The load is 50 Ohms.



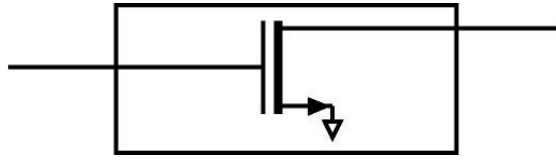
If we directly connect the generator and load to the transistor, what RF power will be delivered to the load ?

RF power delivered to the load = \_\_\_\_\_

part c, 5 points

At 100 GHz, the transistor has  
 $S_{11} = -1/2$ ,  $S_{21} = -4$ ,  $S_{12} = 0$ ,  $S_{22} = +1/3$ ,  
(S-parameters using  $50\Omega$  normalization)

The generator has  $(250/3)$  Ohms source impedance and 1 mW available power. The load is  $(50/3)$  Ohms.



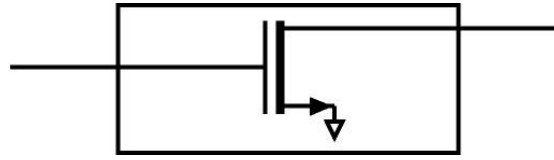
If we impedance-match the generator to the transistor input, but directly connect the load to the transistor output, what RF power will be delivered to the load ?

RF power delivered to the load = \_\_\_\_\_

part d, 5 points

At 100 GHz, the transistor has  
 $S_{11} = -1/2$ ,  $S_{21} = -4$ ,  $S_{12} = 0$ ,  $S_{22} = +1/3$ ,  
(S-parameters using  $50\Omega$  normalization)

The generator has  $(250/3)$  Ohms source impedance and 1 mW available power. The load is  $(50/3)$  Ohms.

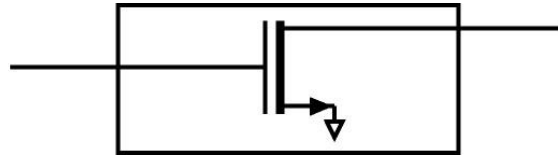


If we place impedance-matching networks between the generator and the transistor, and between the transistor and the load, what RF power will be delivered to the load ?  
RF power delivered to the load = \_\_\_\_\_

part e, 5 points

At 100 GHz, the transistor has  
 $S_{11} = -1/2$ ,  $S_{21} = -4$ ,  $S_{12} = 0$ ,  $S_{22} = +1/3$ ,  
(S-parameters using  $50\Omega$  normalization)

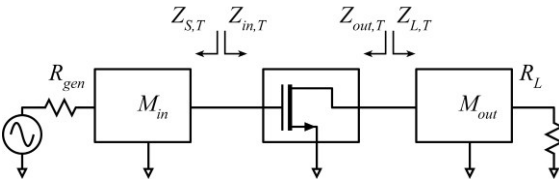
The generator has  $(250/3)$  Ohms source impedance and 1 mW available power. The load is  $(50/3)$  Ohms.



If we directly connect the generator and load to the transistor, what RF power will be delivered to the load ?

RF power delivered to the load = \_\_\_\_\_

part f, 10 points

<p>At 100 GHz, the transistor has  <math>S_{11} = (1/2 + j/2)</math> ← <b>note the change !</b>  <math>S_{21} = -4</math>, <math>S_{12} = 0</math>, <math>S_{22} = +1/3</math>, (S-parameters using <math>50\Omega</math> normalization)</p> <p>The generator has 50 Ohms source impedance and 1 mW available power. The load is 50 Ohms.</p>	
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We impedance-match the generator to the transistor input and impedance-match the load to the transistor output .

Please find the following:

Input impedance of the transistor  $Z_{in,T} =$  \_\_\_\_\_

Source impedance presented to the transistor  $Z_{S,T} =$  \_\_\_\_\_

Output impedance of the transistor  $Z_{out,T} =$  \_\_\_\_\_

Load impedance presented to the transistor  $Z_{L,T} =$  \_\_\_\_\_

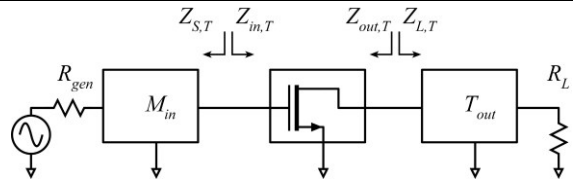




part g. 10 points (218A only)

At 100 GHz, the transistor has  $S_{11}=0$ ,  $S_{21}=4$ ,  $S_{12}=1/8$ ,  $S_{22}=1/3$ ; ← **note the changes !** (S-parameters using  $50\Omega$  normalization)

The generator has  $R_{gen} = 50$  Ohms source impedance. The load is  $R_L = 50$  Ohms.



We are designing a \*power amplifier\*. We have independently determined from  $V_{max}$ ,  $V_{min}$ ,  $I_{max}$ , etc., that the optimum large-signal transistor load impedance is  $Z_{L,T}=200\Omega$  and that the maximum output power, at clipping, is 100 mW. We impedance-match on the input.

Please find the following:

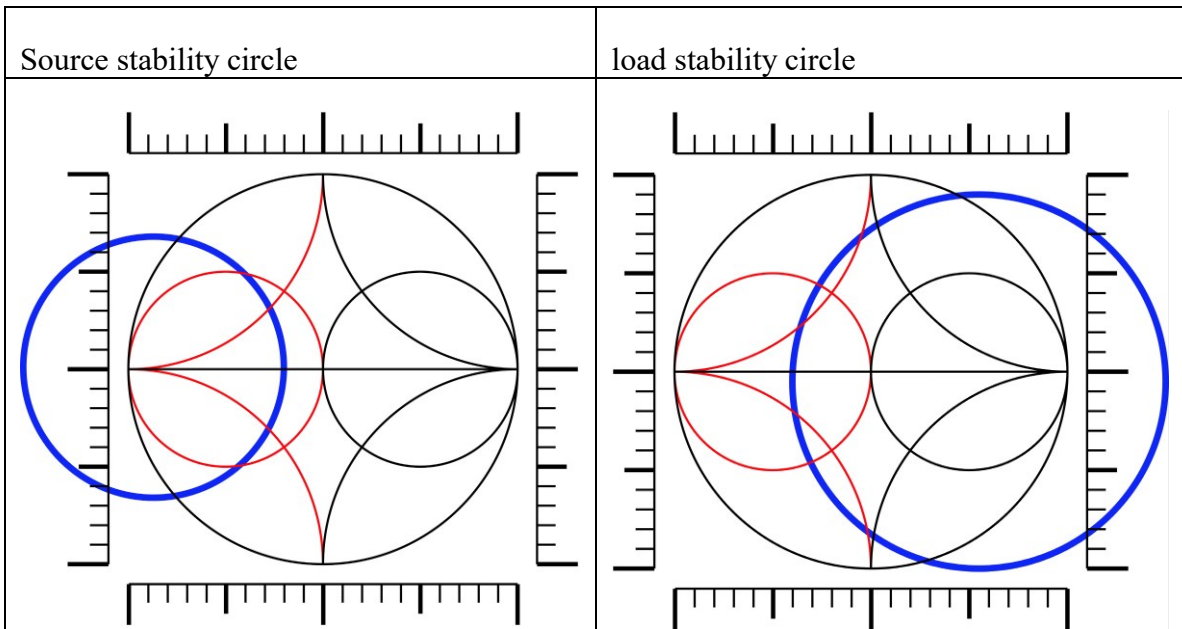
Available generator power at which the amplifier reaches clipping = \_\_\_\_\_

**\*\*This will required some hard thinking\*\***



**Problem 2, 10 points**

*Stabilization*



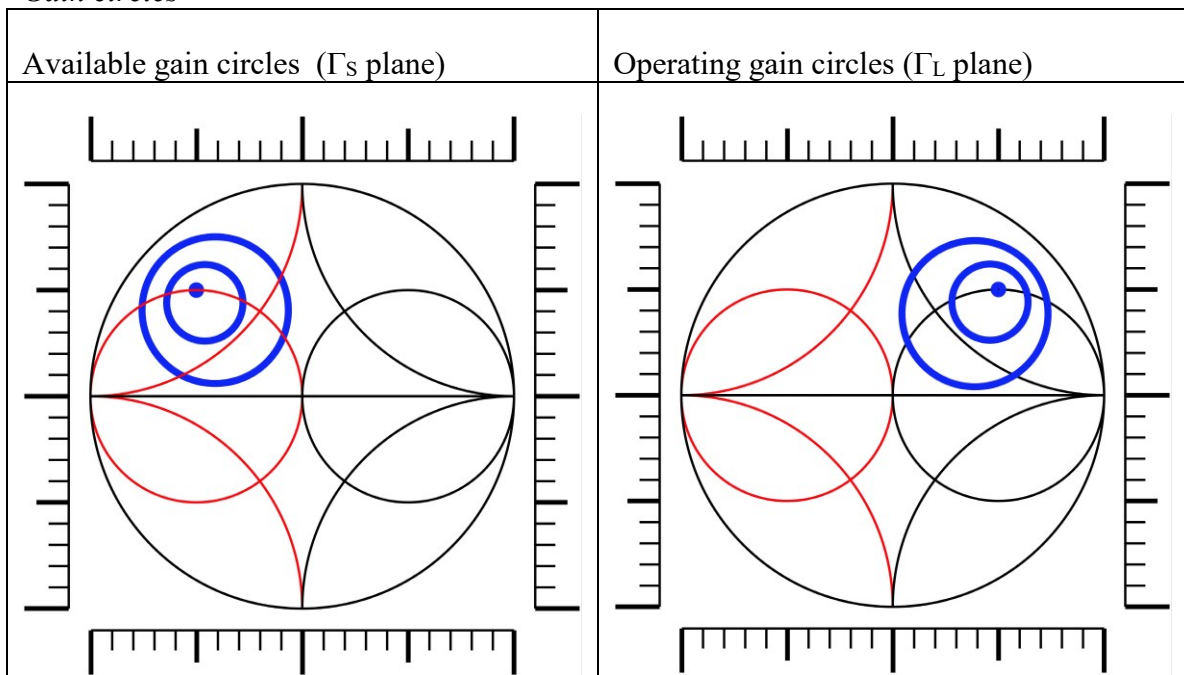
A MOSFET in common-source mode has  $\|S_{11}\| < 1$  and  $\|S_{22}\| < 1$ . Source and load stability circles are as shown. The Smith charts use 50 Ohms impedance normalization. Draw **\*\*2\*\*** circuit diagrams, giving resistor values, of methods of stabilizing the transistor. ***Please draw your answers in the 2 boxes below***

circuit #1	circuit #2
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**Problem 3, 10 points**

*Gain circles*



A FET in common-source mode has operating and available gain circles as shown (50 Ohm impedance normalization). Find the optimum generator and load impedances (in complex Ohms).

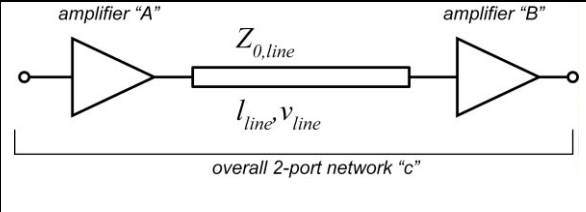
optimum source impedance= \_\_\_\_\_

optimum load impedance= \_\_\_\_\_



**Problem 4, 10 points (145A), 20 points (218A)**  
*2-port parameters and signal flow graphs*

Part a, 10 points

<p>Amplifiers A and B have S-parameters</p> $S_{ij}^A = \begin{bmatrix} 0 & 0 \\ 2 & 1/2 \end{bmatrix} \text{ and } S_{ij}^B = \begin{bmatrix} 1/2 & 0 \\ 2 & 0 \end{bmatrix}.$ <p>(S-parameters using <math>50\Omega</math> normalization).  <math>Z_{o,line} = 50\Omega</math>, <math>l_{line} / v_{line} = \tau_{line} = 1 \text{ nS}</math>.</p>	 <p>The diagram shows an overall 2-port network 'c' enclosed in a box. It consists of three components in series: amplifier 'A' (represented by a triangle pointing right), a transmission line (represented by a rectangle), and amplifier 'B' (represented by a triangle pointing left). The transmission line is labeled with <math>Z_{0,line}</math> above it and <math>l_{line} / v_{line}</math> below it. The input and output ports are indicated by small circles on the left and right respectively.</p>
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Compute  $S_{21}^C$  as a function of frequency. (hint: first draw a signal flow graph)



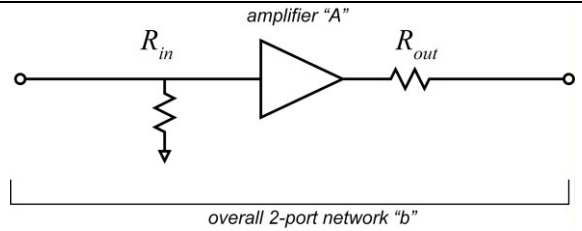


Part b, 10 points (218a only)

Amplifier A has S-parameters

$$S_{ij}^A = \begin{bmatrix} 0 & 1/4 \\ 2 & 1/2 \end{bmatrix}.$$

(S-parameters using  $50\Omega$  normalization).  
Resistors  $R_{in} = 50\Omega$  and  $R_{out} = 50\Omega$  are added in parallel to the input and in series to the output.



Compute  $S_{21}^B$  (hint: first draw a signal flow graph)





**Problem 5, 5 points (145A), 15 point (218A)**

*Power amplifier design*

part a, 5 points

Teledyne's 250nm node InP HBT (heterojunction bipolar transistor) technology has a maximum safe current of 1 mA per micrometer of emitter finger length. For wide bandwidth (high  $f_{max}$ ), the maximum emitter finger length is 5.0 micrometers; set the emitter length at this value, but use multiple emitter to further increase maximum output current to some desired value. The maximum safe collector-emitter voltage is 4.5 V, and the minimum (knee) voltage is 0.5 Volts.

What is the maximum RF power per 1 micron of emitter finger length ?

Power (1 micron)= \_\_\_\_\_

We seek to design a multi-finger HBT cell layout that interfaces to 50 Ohms, with some parallel inductance to tune out the HBT output capacitance.

How many 5 micrometer length emitter fingers would that cell use ? \_\_\_\_\_

What is the maximum output power of that cell ? \_\_\_\_\_

What would be the collector efficiency ? \_\_\_\_\_





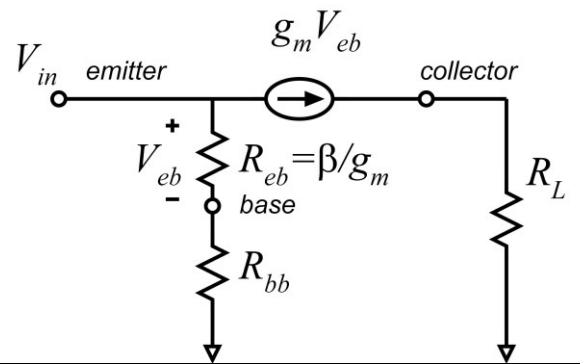
part b, 10 points (218A only)

The transistor is now modelled by the the equivalent circuit to the right.

$$g_m = (1 \text{ mA}/\mu\text{m} \cdot q / kT) \cdot (\text{emitter length}) \cdot (\text{number emitter fingers})$$

$$\beta = 25$$

$$R_{bb} = 10 / g_m$$



Given the 50 Ohm load, the 5 micron emitter length, and the number of emitter fingers you have found earlier, what input power is necessary to produce this maximum output power ?

