

Final Exam, ECE 137A

Thursday March 20, 2025, Noon- 3 p.m.

Name: Solution

Closed Book Exam:

Class Crib-Sheet and 2 pages (4 surfaces) of student notes permitted

Do not open this exam until instructed to do so. Use any and all reasonable approximations (5% accuracy), *after stating & justifying them*.

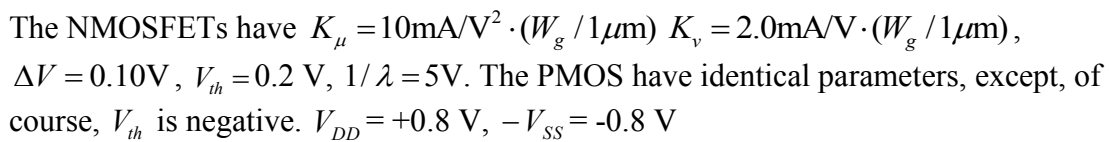
Show your work:

Full credit will not be given for correct answers if supporting work is missing.

Good luck

Part	Points Received	Points Possible	Part	Points Received	Points Possible
1a		5	2b		5
1b		5	2c		15
1c		5	2d		10
1d		12	3a		5
1e		8	3b		10
1f		10	3c		5
2a		5			
total		100			

This is an NOT an Op-Amp: Analyze under the assumption that the differential and common mode input voltages are at zero volts.

 $R_L = 10 \text{ k}\Omega.$

Part a, 5 points

DC bias

Find the following:

Gate width of M2 =

0.189 μm

Gate width of M3 =

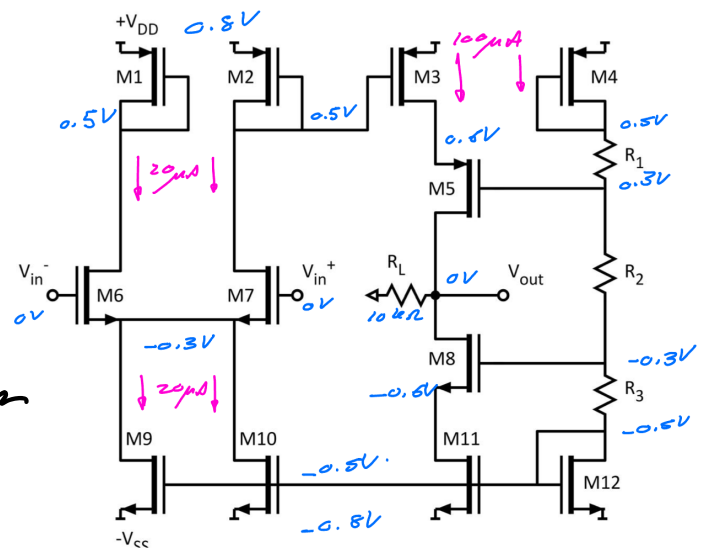
0.96 μm

Value of R_1 =

2 k Ω

Value of R_2 =

6 k Ω



The NMOSFETs have $K_n = 10 \text{ mA/V}^2 \cdot (W_g / 1 \mu\text{m})$, $K_p = 2.0 \text{ mA/V}^2 \cdot (W_g / 1 \mu\text{m})$, $\Delta V = 0.10 \text{ V}$, $V_{th} = 0.2 \text{ V}$, $1/\lambda = 5 \text{ V}$. The PMOS have identical parameters, except, of course, V_{th} is negative. $V_{DD} = +0.8 \text{ V}$, $-V_{SS} = -0.8 \text{ V}$

All transistors have $|V_{gs}| = 0.3 \text{ V}$.

M1,2,6,7,9,10 are biased at $I_D = 20 \mu\text{A}$.

M3,5,8,11,4,12 are biased at $I_D = 100 \mu\text{A}$.

The IR voltage drops across R_1 and R_3 are each 200 mV .

$R_L = 10 \text{ k}\Omega$.

M2 $V_{gs} = V_{ds} = 0.3 \text{ V}$

$$I_D = K_n (V_{gs} - V_{th})^2 (1 + \lambda V_{ds})$$

$$20 \mu\text{A} = K_n (0.1 \text{ V})^2 (1 + 0.3 \text{ V} / 5 \text{ V})$$

$$20 \mu\text{A} = K_n (0.1 \text{ V})^2 (1.06)$$

$$K_n = 20 \mu\text{A} (100) (\text{V}^2) / 1.06 = 1.89 \mu\text{A/V}^2$$

$$1.89 \mu\text{A/V}^2 = 10 \mu\text{A/V}^2 \cdot W_g / 1 \mu\text{m} \rightarrow W_g = 0.189 \mu\text{m}$$

M3 $V_{GS} = 0.2V$, $V_{DS} = 0.2V$

$$I_D = K_M (V_{GS} - V_{TL})^2 (1 + \lambda V_{DS})$$

$$100 \mu A = K_M (0.1V)^2 (1 + 0.2V/5V)$$

$$100 \mu A = K_M (0.1V)^2 (1.04)$$

$$K_M = 100 \mu A (100) (V^2)^{-1} / 1.04 = 9.6 \text{ mA/V}^2$$

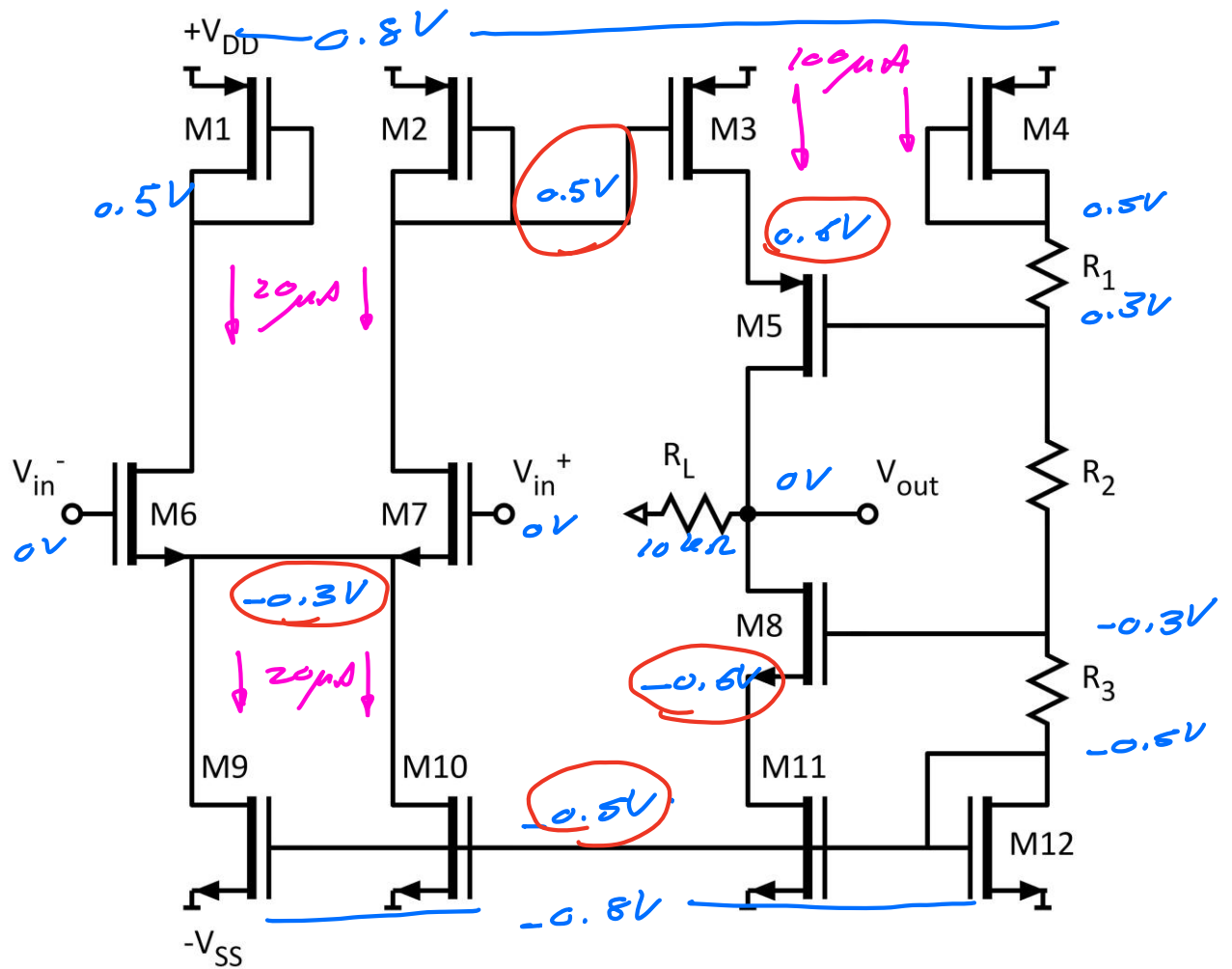
$$9.6 \text{ mA/V}^2 = 10 \text{ mA/V}^2 \cdot W_L / 1 \mu m \rightarrow W_L = 0.96 \mu m$$

1/2 $R_1 = \frac{0.2V}{100 \mu A} = \frac{2V}{1 \text{ mA}} = 2 \text{ k}\Omega$

1/2 $R_2 = \frac{0.6V}{100 \mu A} = 6 \text{ k}\Omega$

Part b, 5 points

DC bias



On the circuit diagram above, label the DC voltages at ALL nodes.

1 pt each for #
circled #5

Part c, 5 points

Find the following

MOSFET M6

MOSFET M7

MOSFET M2

MOSFET M3

MOSFET M5

MOSFET M8

MOSFET M11

$$\left[\begin{array}{ll} g_m = 0.4 \text{ mS} & R_{DS} = 250 \text{ k}\Omega \\ g_m = 0.4 \text{ mS} & R_{DS} = 250 \text{ k}\Omega \\ g_m = 0.4 \text{ mS} & R_{DS} = 250 \text{ k}\Omega \\ g_m = 2 \text{ mS} & R_{DS} = 50 \text{ k}\Omega \\ g_m = 2 \text{ mS} & R_{DS} = 50 \text{ k}\Omega \\ g_m = 2 \text{ mS} & R_{DS} = 50 \text{ k}\Omega \\ g_m = 2 \text{ mS} & R_{DS} = 50 \text{ k}\Omega \end{array} \right]$$

1.25 pts for each group of answers.

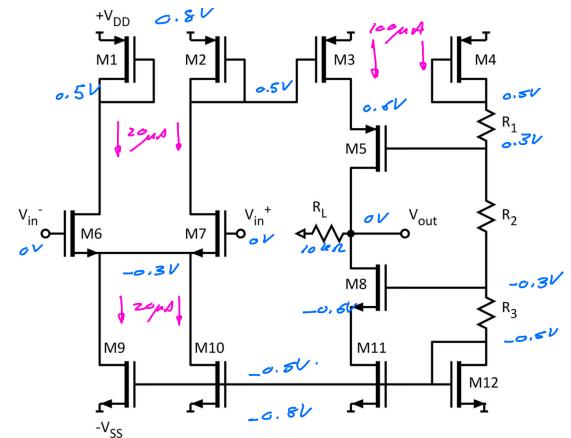
all FETs μ limited.

$$g_m = 2I_D / (V_{GS} - V_{th})$$

$$= 2I_D / 0.1 \text{ V}$$

$$R_{DS} = 1 / \lambda I_D$$

$$= 5 \text{ V} / I_D$$



On the circuit diagram above, label the DC voltages at ALL nodes.

The NMOSFETs have $K_n = 10 \text{ mA/V}^2 \cdot (W/L)$, $K_p = 2.0 \text{ mA/V}^2 \cdot (W/L)$, $\Delta V = 0.10 \text{ V}$, $V_{th} = 0.2 \text{ V}$, $1/\lambda = 5 \text{ V}$. The PMOS have identical parameters, except, of course, V_{th} is negative. $V_{DD} = +0.8 \text{ V}$, $-V_{SS} = -0.8 \text{ V}$.

All transistors have $|V_{GS}| = 0.3 \text{ V}$.

M1,2,6,7,9,10 are biased at $I_D = 20 \text{ }\mu\text{A}$.

M3,5,8,11,4,12 are biased at $I_D = 100 \text{ }\mu\text{A}$.

The IR voltage drops across R_1 and R_3 are each 200 mV .

$R = 10 \text{ k}\Omega$

Part d, 12 points.

Find the following

	Voltage Gain	Input impedance
Transistor combination M3,5,8,11	-20	$\infty \Omega$

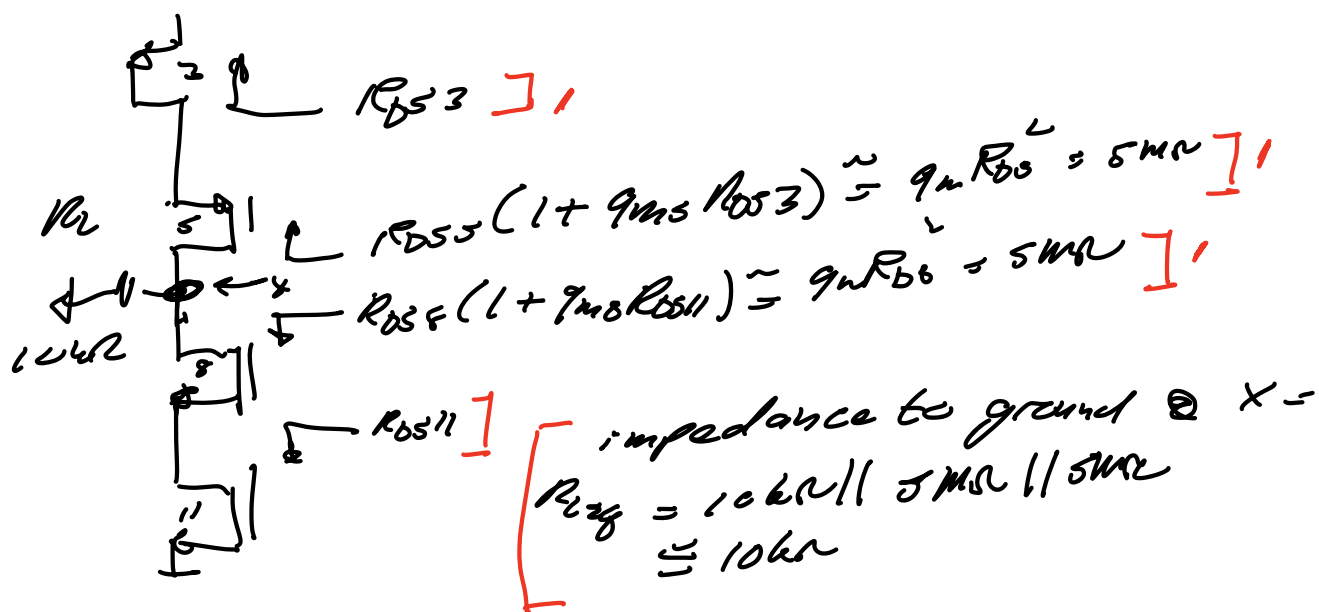
Note: You can analyze M3 and M5 as separate stages, or as a combined stage using Norton/Thevenin methods. Don't ask for hints as to how to do this.

1st way of working

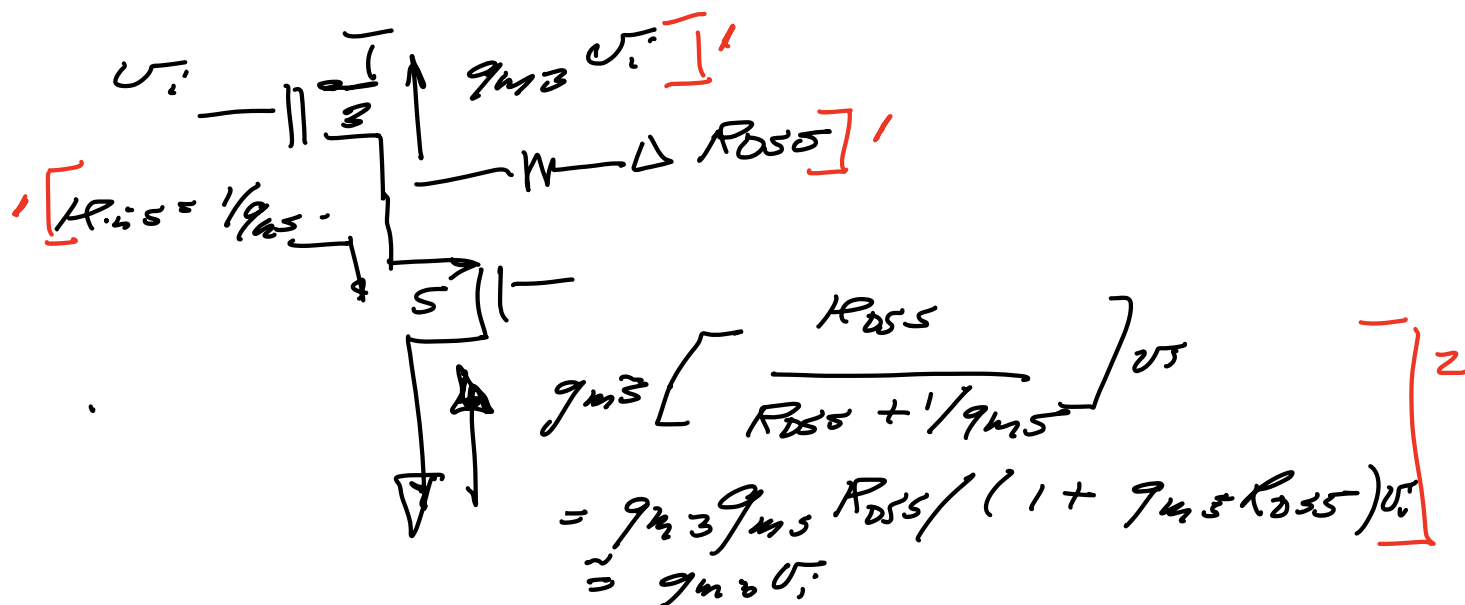
step by step:

$$\begin{aligned}
 &1 \left[R_{out11} = R_{DS11} = 50 \text{ k}\Omega \right. \\
 &2 \left[R_{out8} = R_{DS8} (1 + g_{m8} R_{DS4}) = 5.05 \text{ M}\Omega \right. \\
 &1 \left[R_{eq5} = R_L \parallel R_{out8} = 10 \text{ k}\Omega \parallel 5.05 \text{ M}\Omega = 9.99 \text{ k}\Omega \approx 10 \text{ k}\Omega \right. \\
 &2 \left[R_{in5} = 1/g_{m5} \left(\frac{R_{eq5} + R_{DS5}}{R_{DS5}} \right) = 500 \Omega \left[\frac{10 \text{ k}\Omega + 50 \text{ k}\Omega}{50 \text{ k}\Omega} \right] \right. \\
 &\quad = 600 \Omega \\
 &2 \left[A_{v5} = R_{eq5} / R_{in5} = 10 \text{ k}\Omega / 600 \Omega = 16.7 \right. \\
 &1 \left[R_{eq2} = R_{DS2} \parallel R_{in5} = 50 \text{ k}\Omega \parallel 600 \Omega = 593 \Omega \right. \\
 &2 \left[A_{v3} = -g_{m3} R_{eq3} = 2 \text{ mS} \cdot 590 \Omega = -1.19 \right. \\
 &1 \left[A_{v3} A_{v5} = -1.19 \cdot 16.7 = -19.8 \right.
 \end{aligned}$$

warten - though:



short-circuit current



open-circuit voltage = short-circuit current $\times$ Thevenin resistance.

$$= -g_{m3} \cdot R_{zy}$$

$$= -2ms \cdot 10^4 s^{-1} = -20$$

Part e, 8 points.

Find the following

	Voltage Gain	Input impedance
Transistor combination M1,2,6,7,9,10	-0.49	$\infty \Omega$
Overall op-amp $V_{out} / (V_{in}^+ - V_{in}^-)$	9.8	$\infty \Omega$

Hint: although M2 is a diode-connected FET, the small-signal resistance of this 2-terminal element, although mostly determined by the FET transconductance, also has a slightly contribution from the FET R_{DS} .

3

$$R_{eq7} = R_{DS7} \parallel R_{DS2} \parallel 1/g_{m2} =$$

$$= 250k \parallel 250k \parallel 2.13k\Omega$$

$$= 2.45k\Omega$$

-1 pt if R_{DS2} was omitted.

2

$$A_{v62} = -\frac{g_{m2}}{2} \cdot R_{eq7}$$

$$= -0.49$$

2

overall

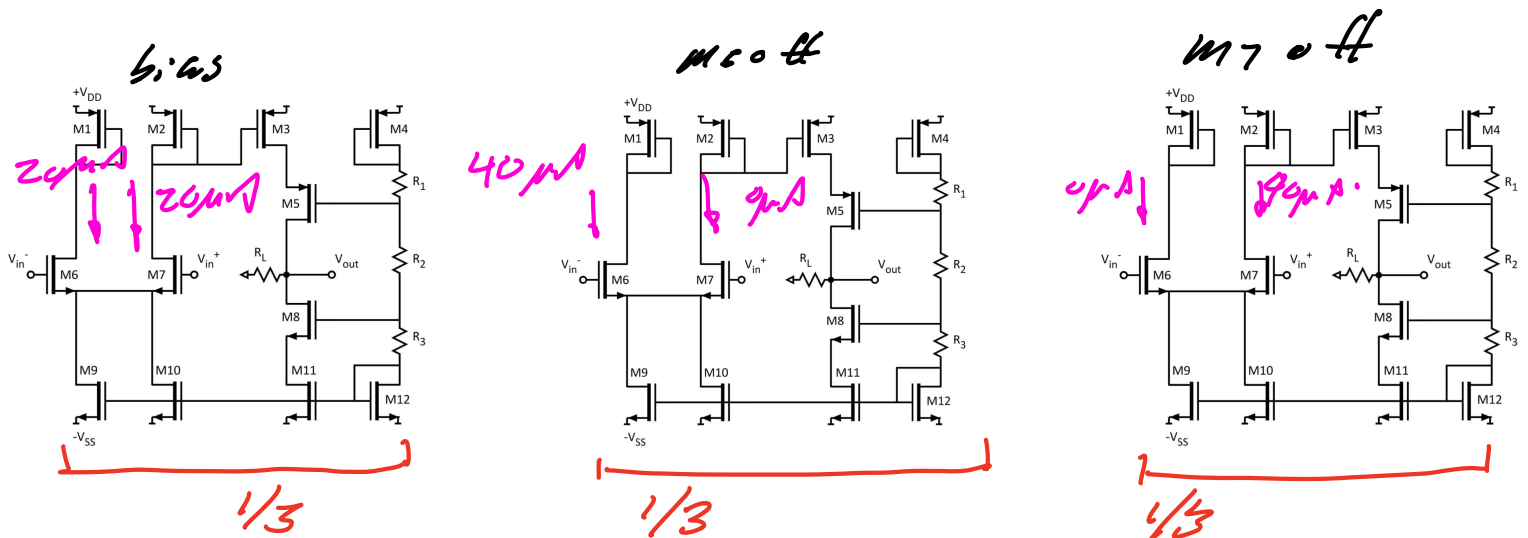
$$A_{voverall} = (-0.49) \cdot (-20)$$

$$= \underline{9.8}$$

Part f, 10 points

Maximum output voltage swings (show all your work).

	magnitude and sign of maximum output signal swing due to <i>cutoff</i>	magnitude and sign of maximum output signal swing due to <i>knee voltage</i>
Transistor M6	$+0.98V$	Do not calculate
Transistor M7	$-0.98V$	Do not calculate
Transistor M3	$-1.0V$	Do not calculate
Transistor M5	Do not calculate	$+0.5V$
Transistor M8	Do not calculate	$-0.5V$



→ maximum change in I_{D7} is $\pm 20\mu A$.

max. change ΔV_{out} of M7 stage is

$$\Delta V_{max, out, m7} = \pm 20\mu A \cdot R_{eq7}$$

$$= \pm 20\mu A \cdot 2.45 k\Omega = \pm 49 mV$$

corresponding $\Delta V_{out} = \pm 49 mV \cdot A_{v3,5}$

$$= \pm 49 mV \cdot 20$$

$$= \pm 0.98 V$$

There are 2 ways of calculating $m3$ cutoff

Solution using Hs from page 8

$m3$ Cutoff: $\Delta I_{D3} = 100 \mu A$]

$$\begin{aligned}\Delta V_{out3} &= 100 \mu A \cdot R_{Leg3} \\ &= 100 \mu A \cdot 600 \Omega \\ &= -60 mV \downarrow\end{aligned}$$

$$\begin{aligned}\Delta V_{out} &= \Delta V_{out3} \cdot A_{vs} = \\ &= (-60 mV)(+16.7) \\ &= -1.0 V\end{aligned}$$

Alternate solution: using Hs from page 9,

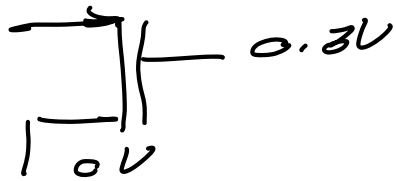
$\Delta I_{D3} = 100 \mu A$]

$$\Delta I_{D5} = \Delta I_{D3} \left[\frac{g_{m3} R_{D55}}{g_{m3} R_{D55} + 1} \right] = 100 \mu A$$
$$= 80 \mu A$$

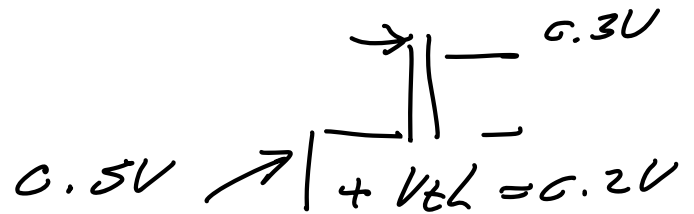
$$\begin{aligned}\Delta V_{out} &= \Delta I_{D5} \cdot 10 k\Omega \\ &= -1.0 V \downarrow\end{aligned}$$

Knee voltage MS

V_{BILS}



Knee

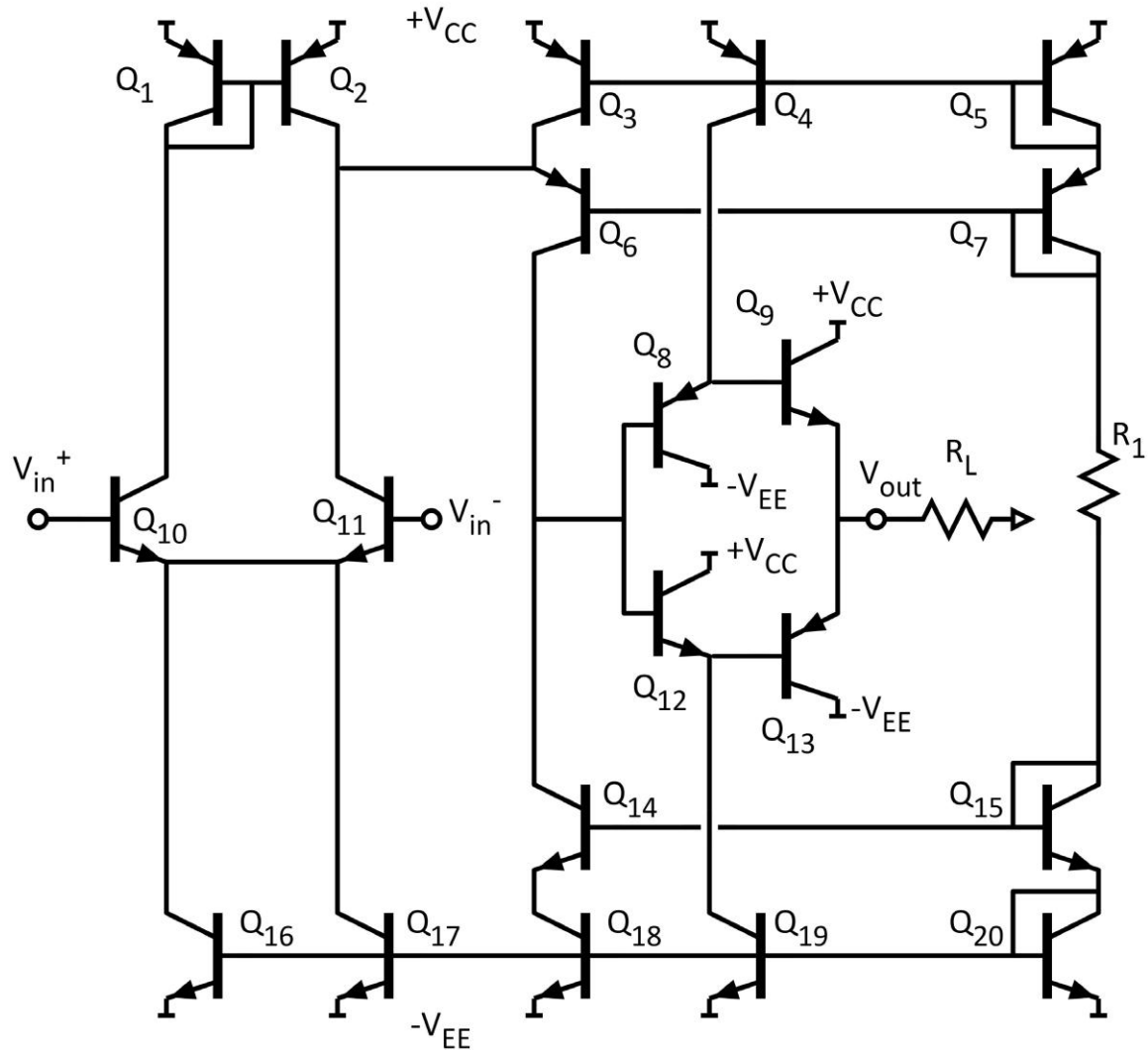


$$\Delta V_{out} = +0.5V \uparrow$$

Knee voltage of MS
 → same calculation, opposite sign
-0.5V

Problem 2, 35 points

This is an Op-Amp---analyze the bias under the assumption that DC output voltage V_{out} is zero volts, that the positive input V_{in+} is zero volts, and that we must determine the DC value of the negative input voltage (V_{in-}) necessary to obtain this.



All the transistors have the same (matched) I_S , have $\beta = \infty$, and $V_A = 100$ Volts.

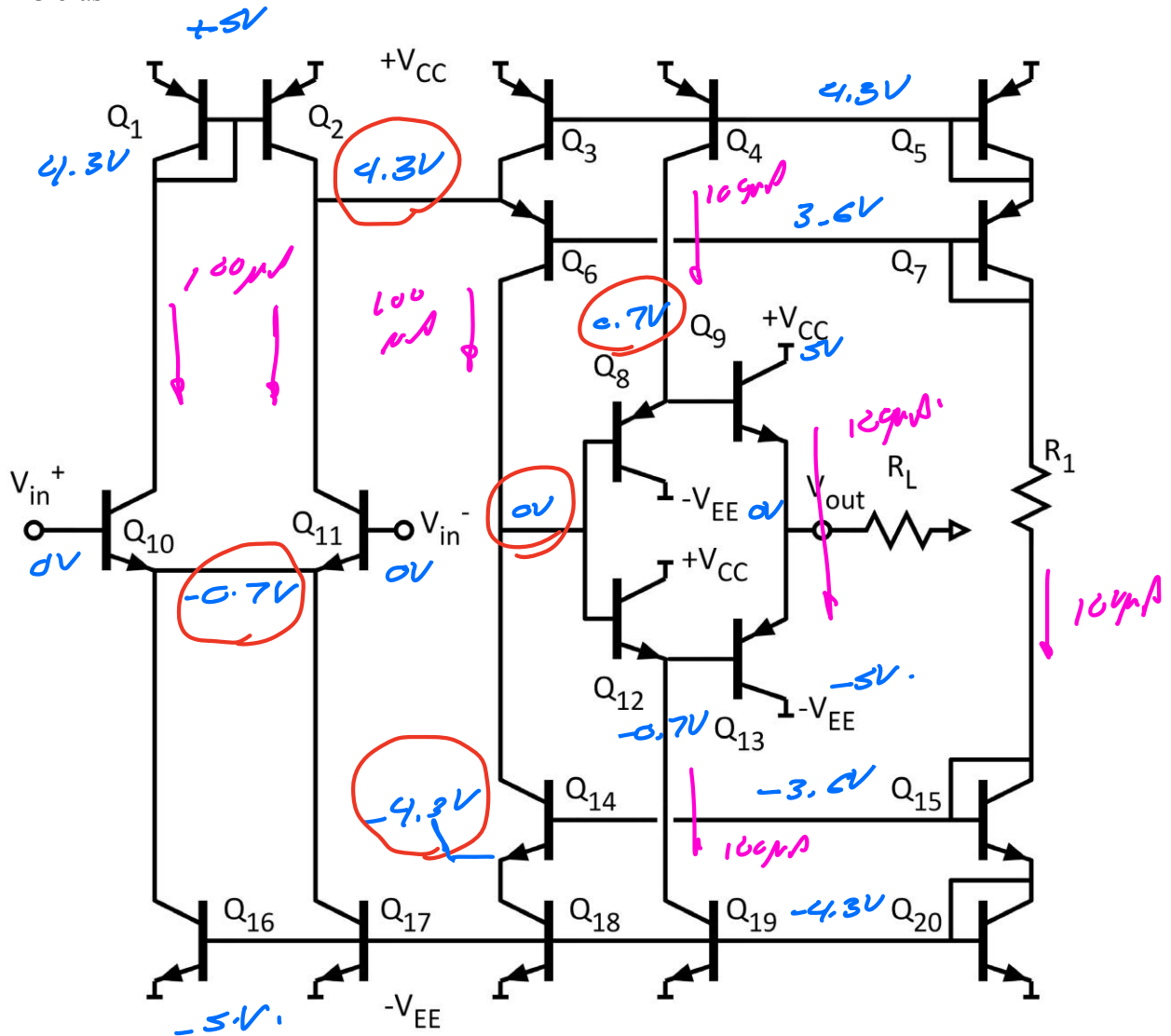
$V_{CE(sat)} = 0.5V$. V_{be} is approximately $0.7V$, but use the exact relationship

$V_{be} = (kT/q) \ln(I_E / I_S)$ when appropriate. The supplies are $+5$ Volts and -5 Volts. All transistors have the same I_S , and all are biased at 0.1 mA collector current.

$R_L = 1$ kOhm.

$R_L = 1 \text{ k}\Omega$.

DC bias



On the circuit diagram above, label the DC voltages at **ALL nodes**.

1 pt each for circled values.

Part b, 5 points.

Find the following

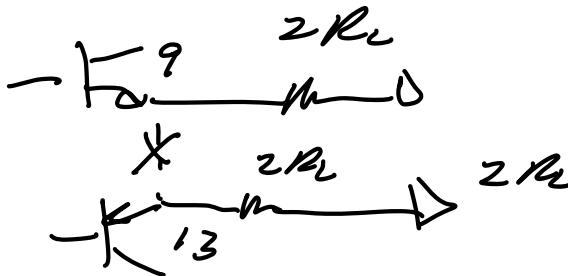
	Voltage Gain	Input impedance
Transistor combination Q8,9,12,13	0.885 or 0.794	$\infty \Omega$

$$R_{E2} = V_{CE} / I_{C2} = 100V / 0.1mA = 1M\Omega \quad 1/g_m = 260\Omega$$

Q9/12 is push/pull: strong + output: Q9 on
strong - output: Q13 on
small signal: both on.

I will work solution for Both on
but all 3 solutions are acceptable.

If Q9 & 13 are both on then we can analyze
like so



$$R_{eq9} = 2k\Omega \parallel R_{CQ9} = 2k\Omega \parallel 1M\Omega \approx 2k\Omega$$

$$\mu_{v9} = 2k\Omega / (2k\Omega + 260\Omega) = 0.885$$

$$R_{i9} = \beta (1/g_m + R_{eq9}) = \infty \Omega.$$

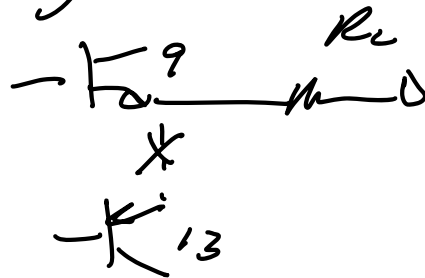
$$R_{eq8} = R_{i9} \parallel R_{eq8} \parallel R_{CE8} = \infty \Omega \parallel 1M\Omega \parallel 1M\Omega = 500k\Omega$$

$$\mu_{v8} = R_{eq8} / (R_{eq8} + 1/g_{m8}) = 0.794 \approx 1$$

$$R_{i8} = \infty \Omega$$

If Q9 is on but Q13 is off

then we can analyze like so



$$R_{eq9} = R_L \parallel R_{eq9} = \infty \parallel 1M\Omega \approx 1M\Omega$$

$$\mu_{v9} = 1M\Omega / (1M\Omega + 260\Omega) = 0.794$$

$$R_{i9} = R_L (1/g_m + R_{eq9}) = \infty \Omega$$

$$R_{eq8} = R_{i9} \parallel R_{eq8} \parallel R_{ce8} = \infty \Omega \parallel 1M\Omega \parallel 1M\Omega = 500k\Omega$$

$$\mu_{v8} = A_{v8} / (R_{eq8} + 1/g_{m8}) = 0.999 \approx 1$$

$$R_{i8} = \infty \Omega$$

You can also work Q13 on, Q9 off
... same analysis...

* depends on answer to part b.

Part c, 15 points.

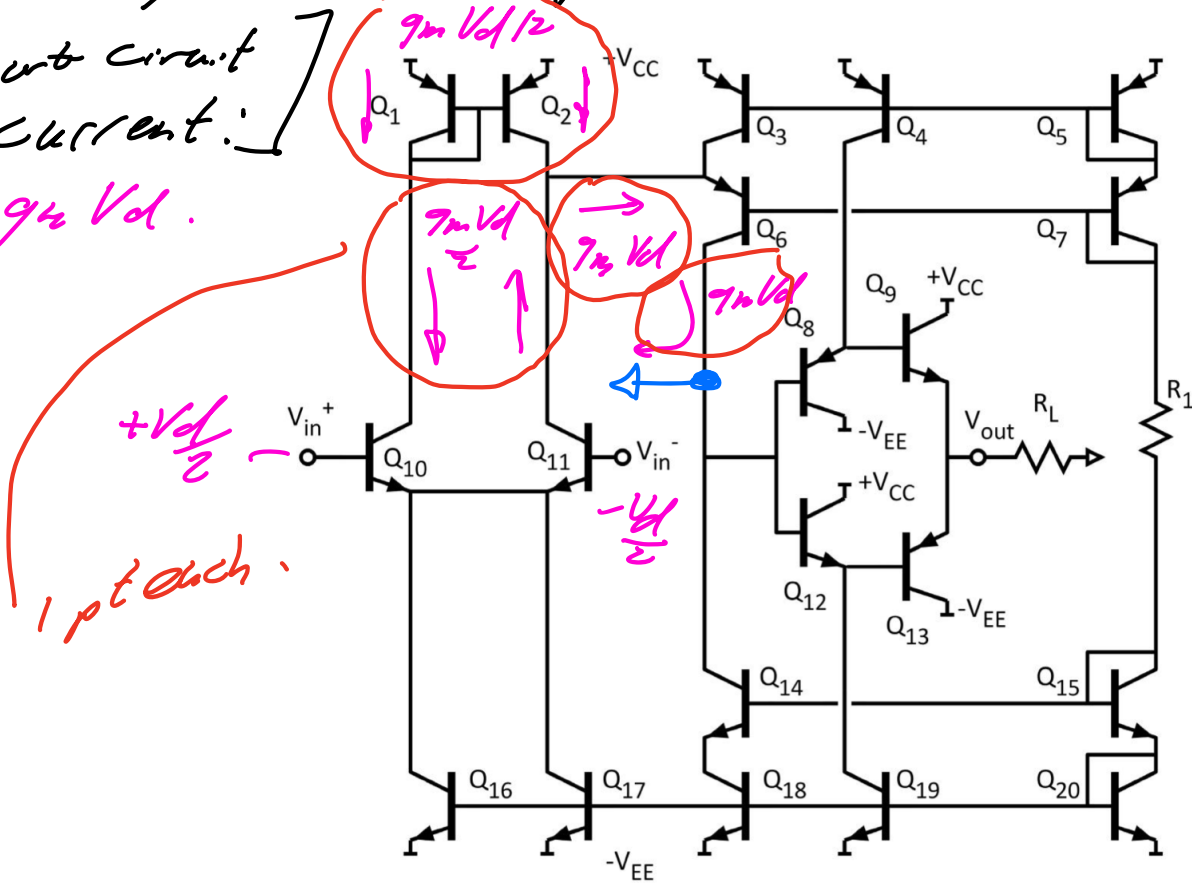
Find the following

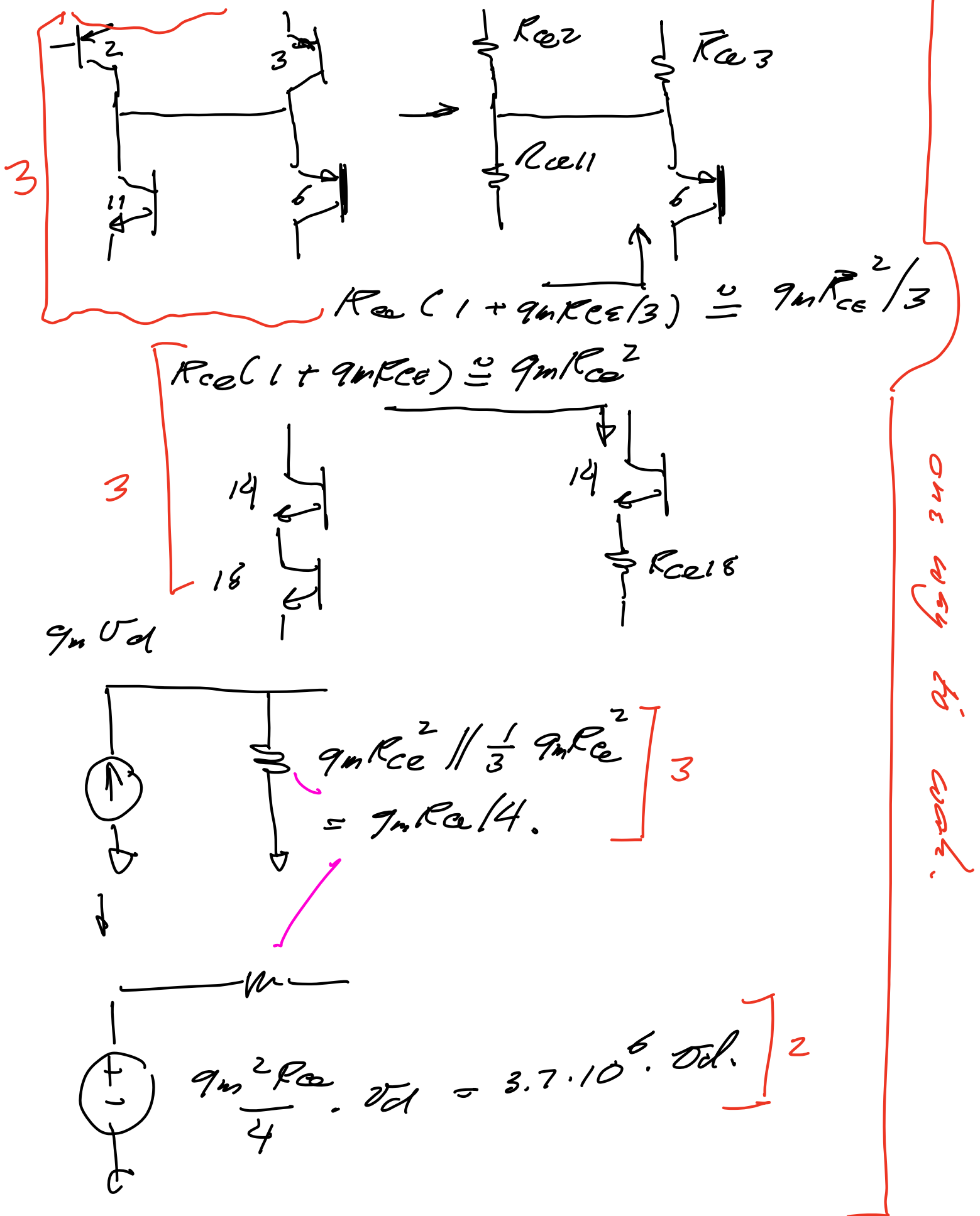
	Voltage Gain	Input impedance
Transistor combination Q1,2,10,11,6	$3.7 \cdot 10^6$	$\infty \Omega$
Overall op-amp $V_{out} / (V_{in}^+ - V_{in}^-)$	$3.3 \cdot 10^6$ or * $2.9 \cdot 10^6$	$\infty \Omega$

Note: You can analyze (Q1,2,10,11) and Q6 as separate stages, or as a combined stage using Norton/Thevenin methods. Don't ask for hints as to how to do this.

using Norton/Thevenin methods:

short circuit
current:
 $= g_m V_d$.





step-by-step method:

$$3 \left[R_{out14} = R_{o14} \cdot (1 + g_{m14} R_{e18}) \right. \\ \left. = g_{m14} R_{e18}^2 \right]$$

$$1 \left[R_{Leg6} = R_{out14} \right. \\ \left. R_{in6} = 1/g_{m6} \left(\frac{R_{Leg6} + R_{e6}}{R_{e6}} \right) \right. \\ 3 \left[= \frac{1}{g_{m6}} \frac{g_{m6} R_{e6}^2}{R_{e6}} = R_{e6} \right]$$

$$2 \left[A_{v6} = R_{Leg6} / R_{in6} = g_{m14} R_{e18}^2 / R_{e6} = g_{m14} R_{e6} \right]$$

$$4 \left[R_{Leg11} = R_{in6} \parallel R_{e3} \parallel R_{e2} \parallel R_{e11} = R_{e14} \right]$$

$$1 \left[A_{v11} = g_{m14} R_{Leg11} = g_{m14} R_{e14} \right]$$

$$1 \left[\text{overall gain} = g_{m14} R_{e14} \cdot g_{m14} R_{e14} / 4 \right. \\ \left. = (g_{m14} R_{e14})^2 / 4 \right. \\ \left. = 3.70 \cdot 10^6 \right]$$

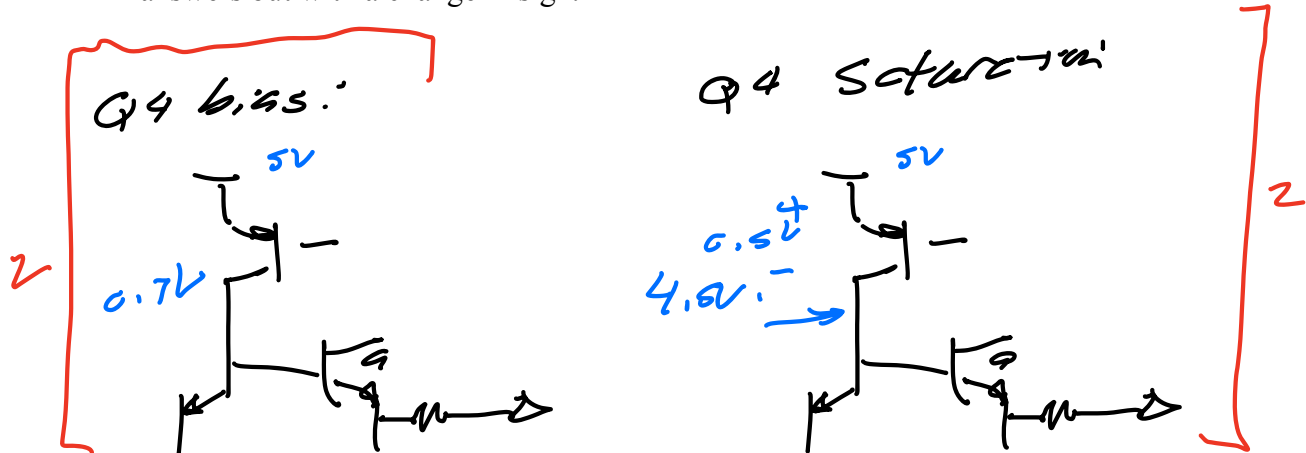
another way to work.

Part d, 10 points

Maximum output voltage swings (show all your work).

	magnitude and sign of maximum output signal swing due to <i>saturation voltage</i> (saturation)
Transistor Q4	3.36V
Transistor Q9	4.5V

Note that transistors Q13 and Q19, Because of the circuit symmetry, Will give similar answers but with a change in sign.

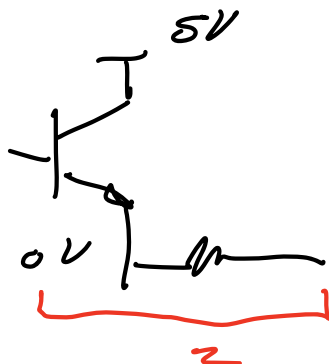


1 [$\Delta V_{b9} = 4.5V - 0.7V = + 3.8V$

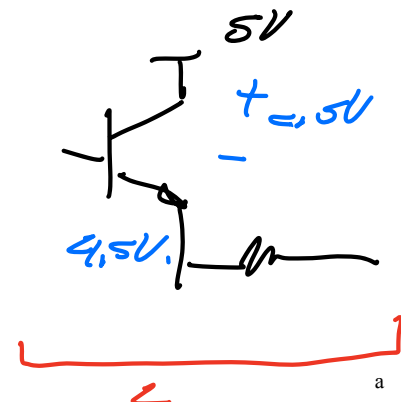
1 [$\Delta V_{out} = 3.8V \cdot A_{v9}$
 $= 3.8V \cdot 0.885$
 $= 3.36V$

ok to use $A_{v9} =$
either
0.885 or 0.794

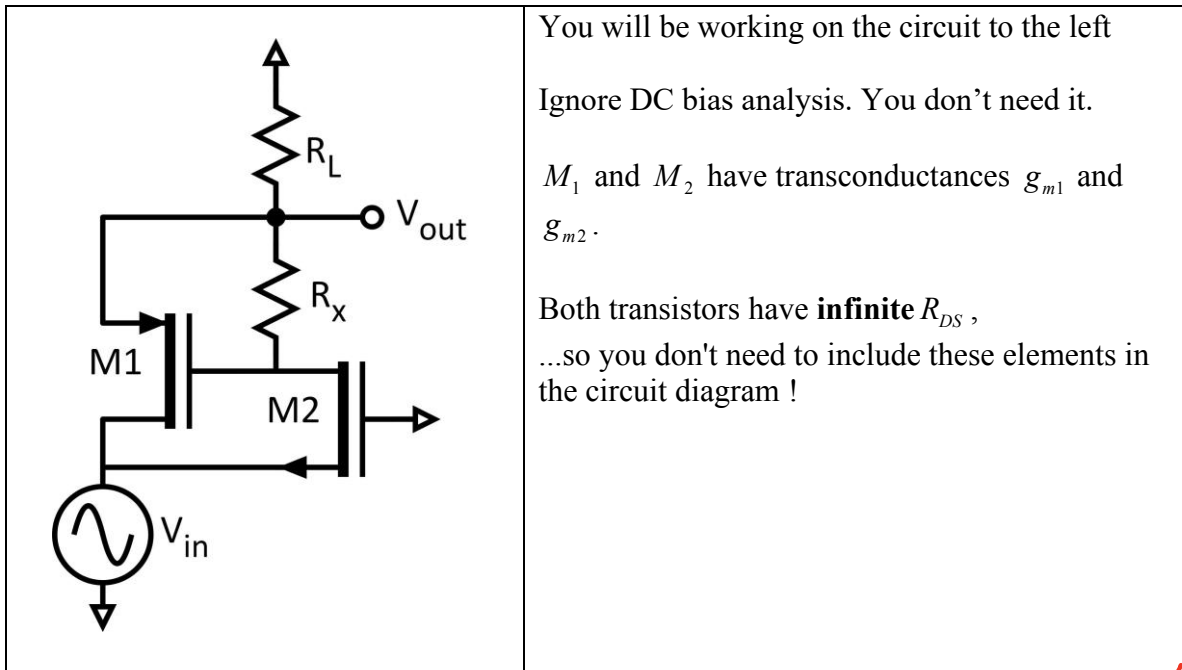
Q9 bias



Q9 saturation



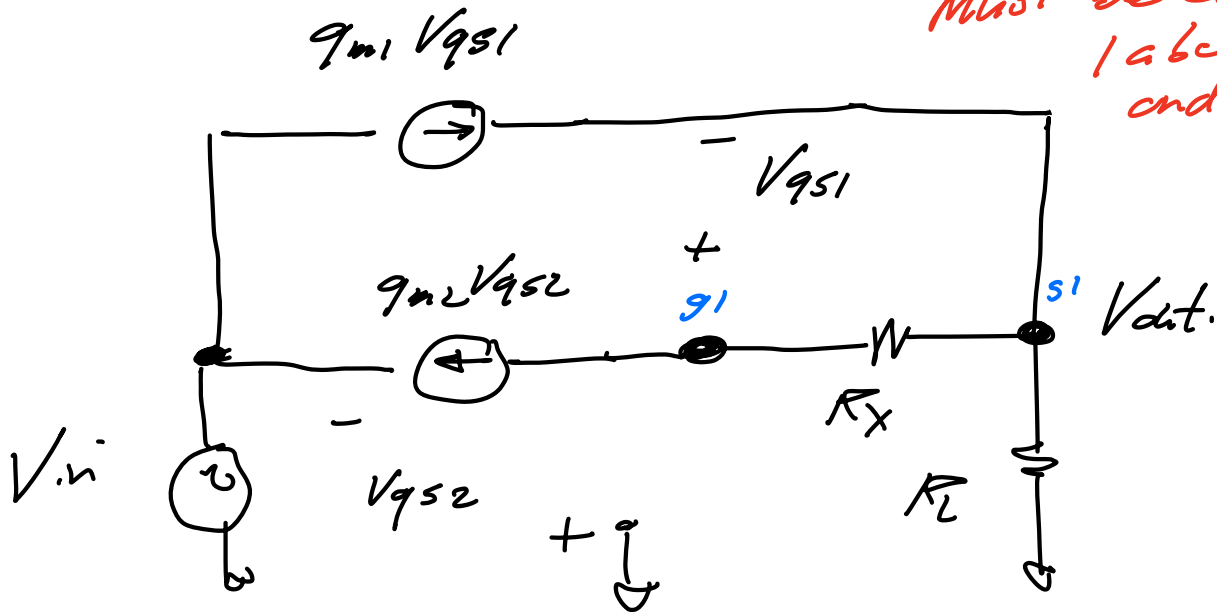
Problem 3, 20 points



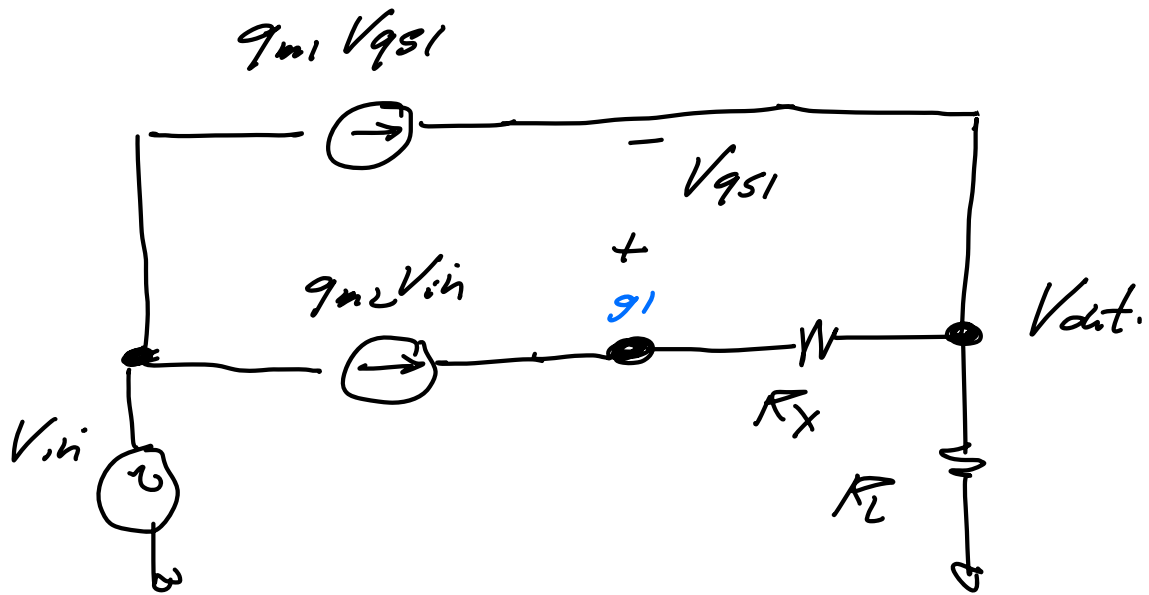
Part a, 5 points

Draw a small-signal equivalent circuit of the circuit.

Voltages controlling g_m generators must be clearly labeled and located.



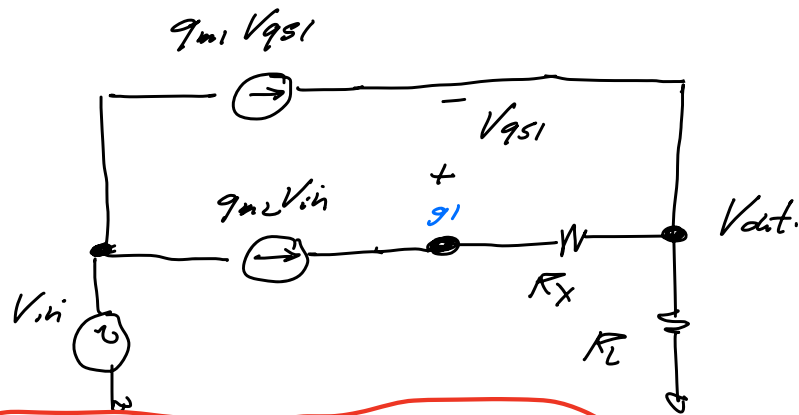
Alternative
answer.



Part b, 10 points

Derive an algebraic expression for V_{out}/V_{in} in terms of g_{m1} , g_{m2} , R_L , and R_X

$$V_{out}/V_{in} = g_{m2} R_L (1 + g_{m1} R_X)$$



$$\sum I = 0 \text{ @ } V_{g1}$$

$$A) -g_{m2} V_{in} + (V_{g1} - V_{out}) / R_X = 0$$

4

$$\sum I = 0 \text{ @ } V_{out}:$$

$$-g_{m1} V_{g1} - (V_{g1} - V_{out}) / R_X + V_{out} / R_L = 0$$

4

$$B) -g_{m1} (V_{g1} - V_{out}) - (V_{g1} - V_{out}) / R_X + V_{out} / R_L = 0$$

From A: $(V_{g1} - V_{out}) = (g_{m2} R_X V_{in})$

or = solution

So from B:

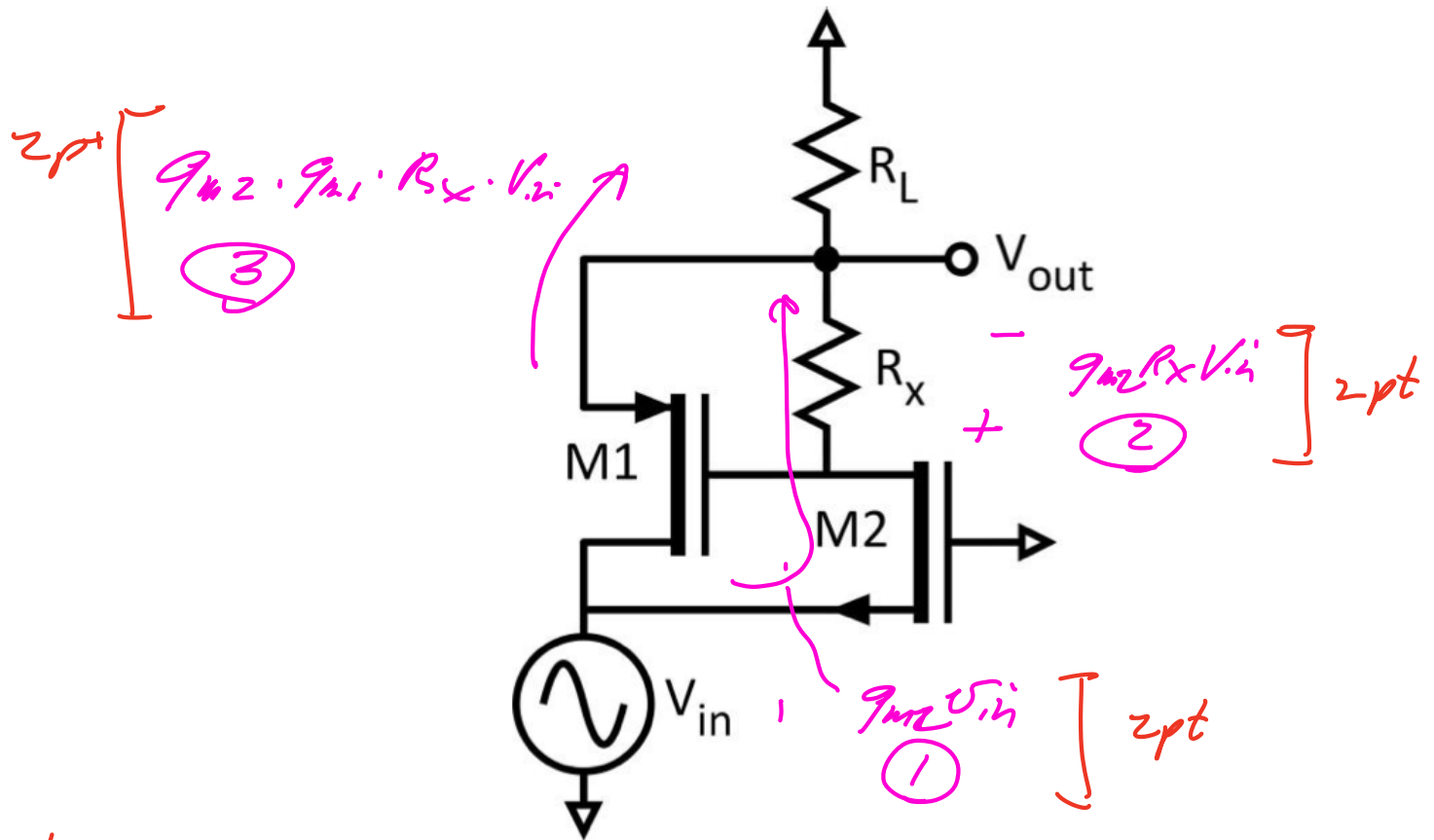
$$-g_{m1}(g_{m2}R_X V_{in}) - (g_{m2}R_X V_{in})/R_X + V_{out}/R_L = 0$$

$$-g_{m1}(g_{m2}R_X V_{in}) - g_{m2}V_{in} + V_{out}/R_L = 0$$

$$V_{out}/R_L = g_{m2} (1 + g_{m1}R_X) V_{in}$$

$$V_{out}/V_{in} = g_{m2}R_L (1 + g_{m1}R_X)$$

OK



Handwritten equation (4):

$$V_{out} = R_L (g_{m2} V_{in} + g_{m1} g_{m2} R_x V_{in})$$

Handwritten equation for the voltage gain:

$$\rightarrow V_{out}/V_{in} = g_{m2} R_L (1 + g_{m1} R_x)$$

2nd solution

Part c, 5 points

Set $g_{m1}=1 \text{ mS}$, $g_{m2}=2 \text{ mS}$, $R_L=3 \text{ k}\Omega$, and $R_X=5 \text{ k}\Omega$.

Find the numerical value of V_{out} / V_{in}

$$V_{out} / V_{in} = 36$$

5 pt.

$$\begin{aligned} A_v &= g_{m2} R_L (1 + g_{m1} R_X) \\ &= 2 \text{ mS} \cdot 3 \text{ k}\Omega (1 + 1 \text{ mS} \cdot 5 \text{ k}\Omega) \\ &= 6 [1 + 5] \\ &= 36 \end{aligned}$$

