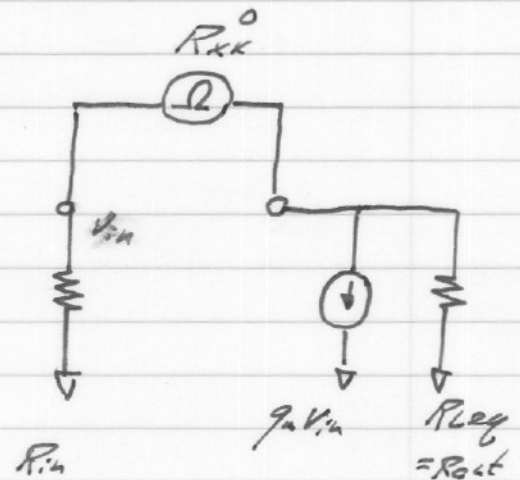
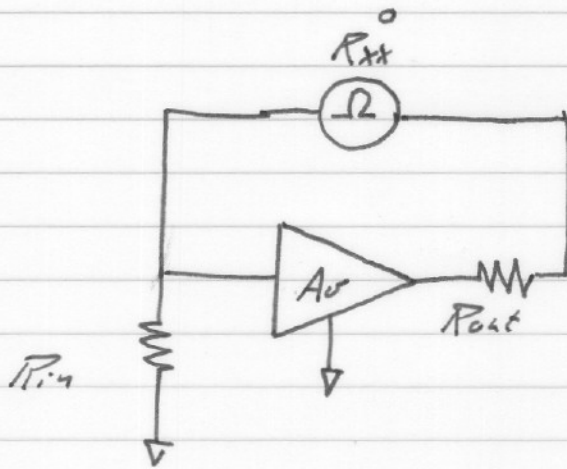


# ECE 13713 Notes set 7:

- 1) MORE Regarding motc,
- 2) Emitter and source follower by motc.

We had earlier found:

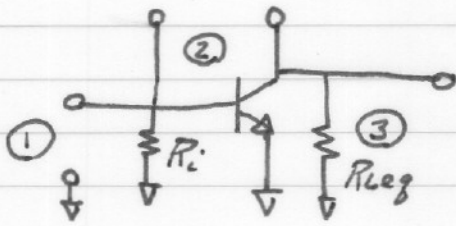


$$R_{xx}^o = R_i [1 - A_v] + R_{out}$$

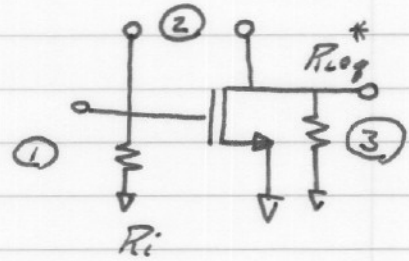
$$R_{xx}^o = R_i [1 + g_m R_{eq}] + R_{eq}$$

this will be useful for source and emitter follower

There are some other useful relationships:



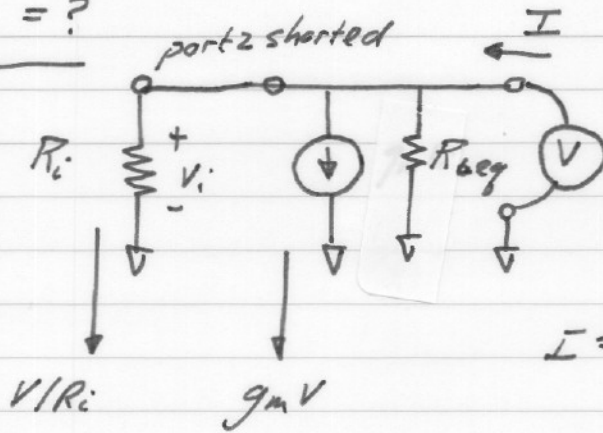
or



\*  $R_i$  includes  $R_{be}$   
 \*  $R_{leg}$  includes  $R_{ce}$

\*  $R_{leg}$  includes  $R_{ds}$

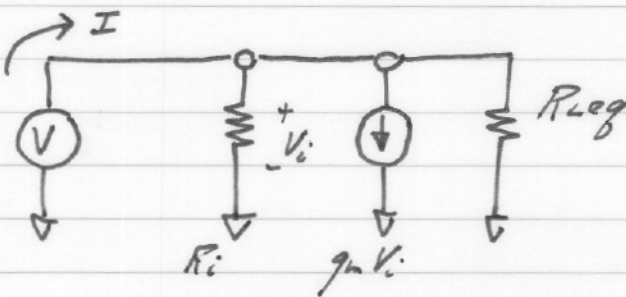
$R_{33}^2 = ?$



$$I = V(g_m + 1/R_i) + V_0/R_{leg}$$

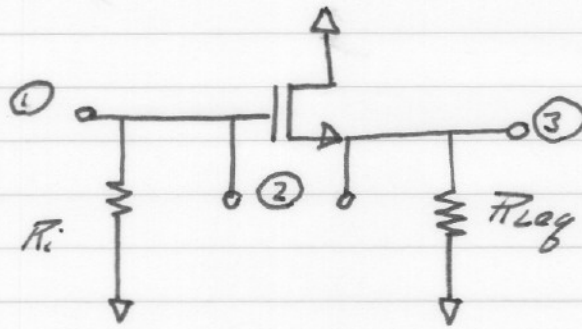
$$\Rightarrow V/I = R_{33}^2 = R_i \parallel \frac{1}{g_m} \parallel R_{leg}$$

$R_{11}^2 = ?$

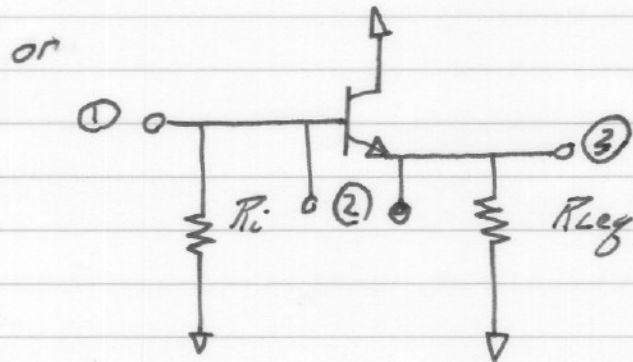


$$I = V(g_m + 1/R_i + 1/R_{leg})$$

$$\Rightarrow R_{11}^2 = R_i \parallel \frac{1}{g_m} \parallel R_{leg}$$

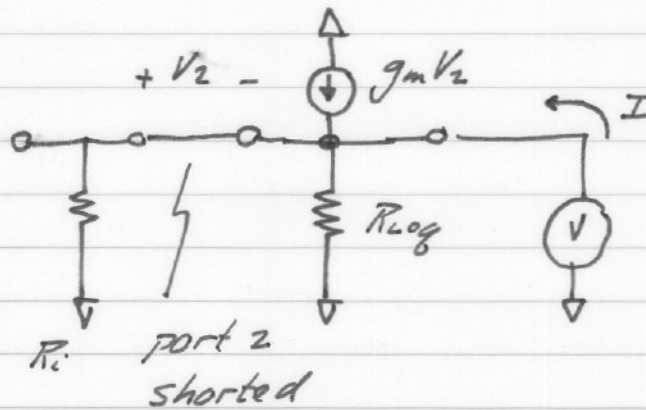


\*  $R_{leg}$  includes  $R_{obs}$



\*  $R_{leg}$  includes  $R_{CE}$

$R_{33}^2 = ?$

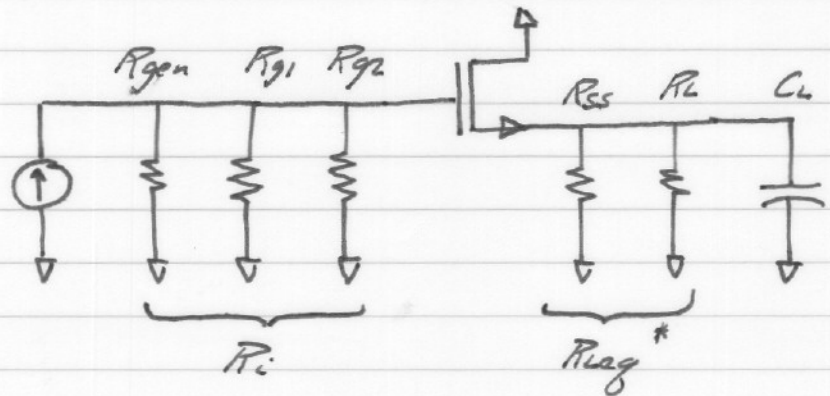
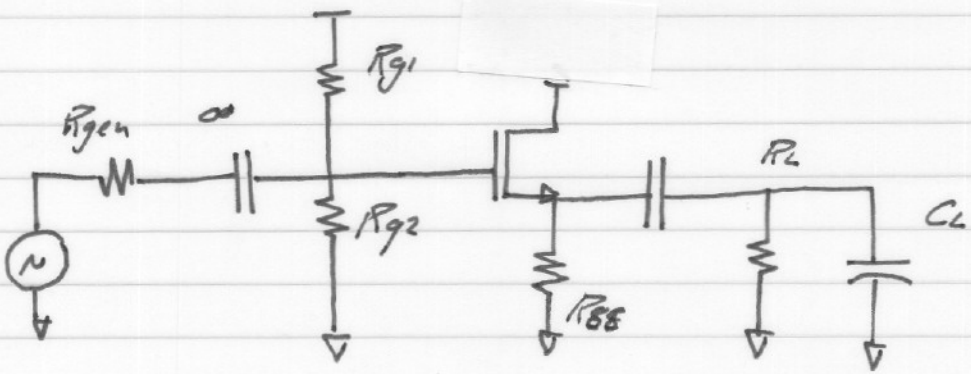


shorting port 2 makes  $V_2 = 0 \Rightarrow g_m V_2 = 0$

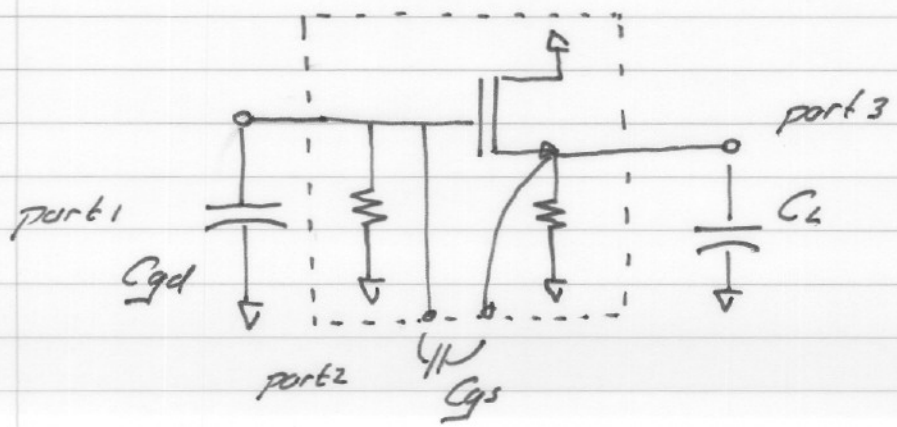
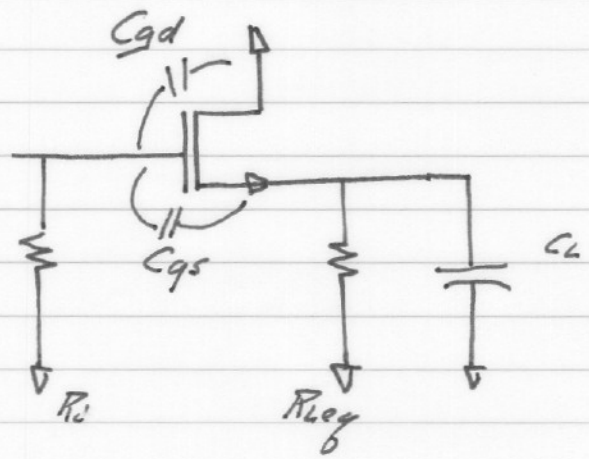
$R_{33}^2 = R_{leg} \parallel R_i$

By a very similar construction,  $R_{11}^2 = R_{leg} \parallel R_i$

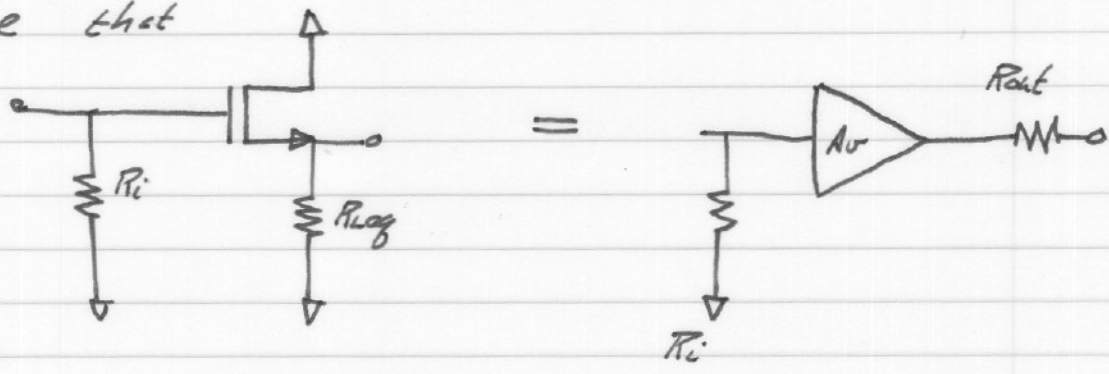
We now can solve the source follower easily



\* $R_{eq}$  includes  $R_{SS}$



note that

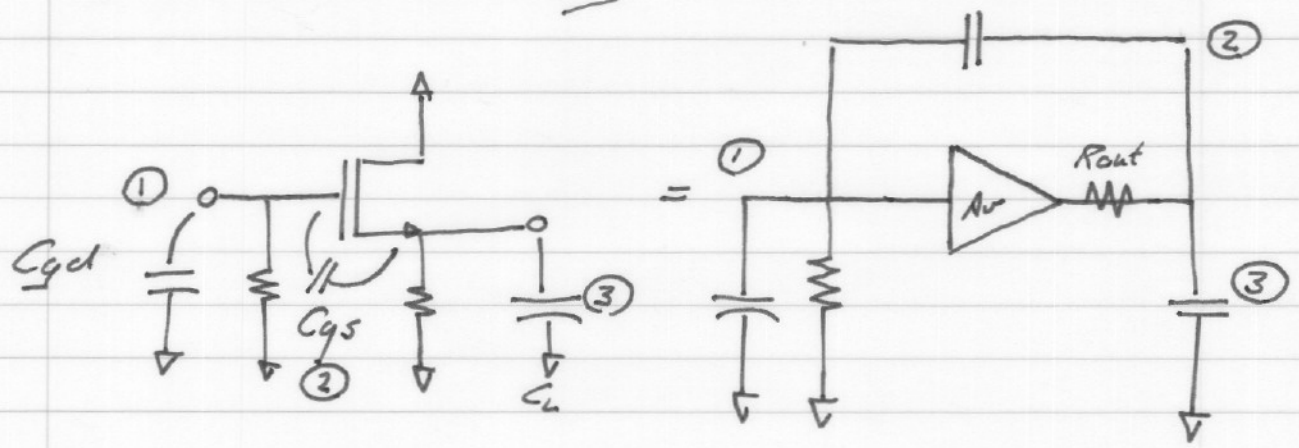


$$R_i = R_{leg}$$

$$A_v = R_{leg} / (R_{leg} + 1/g_m)$$

$$R_{out} = R_{leg} \parallel \frac{1}{g_m}$$

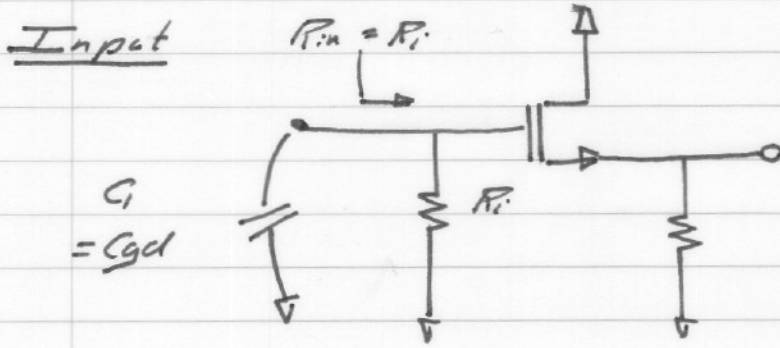
so we can immediately write the time constants:



$$\tau_1 = R_{11}^0 C_1 + R_{22}^0 C_2 + R_{33}^0 C_3$$

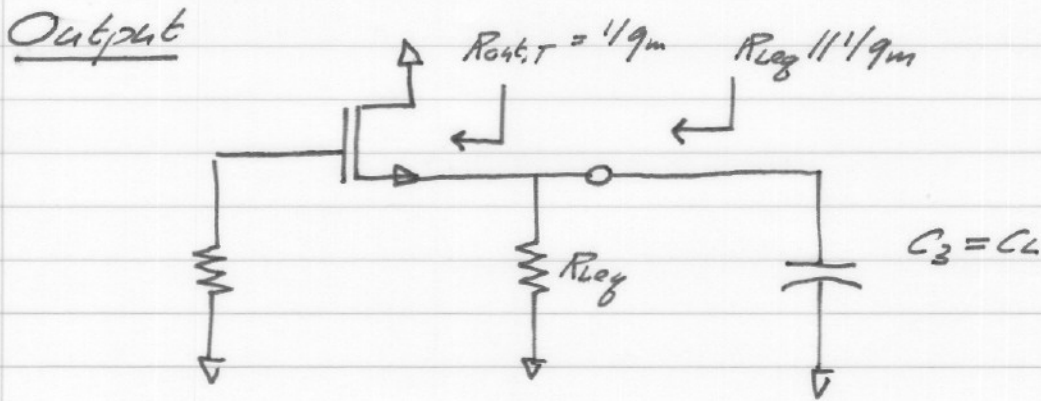
$$= C_{gd} \cdot R_i + C_{gs} \left[ \left( 1 - \frac{R_{leg}}{R_{leg} + 1/g_m} \right) R_i + R_{leg} \parallel \frac{1}{g_m} \right] + C_L \left[ R_{leg} \parallel \frac{1}{g_m} \right]$$

Lets look at those terms again:



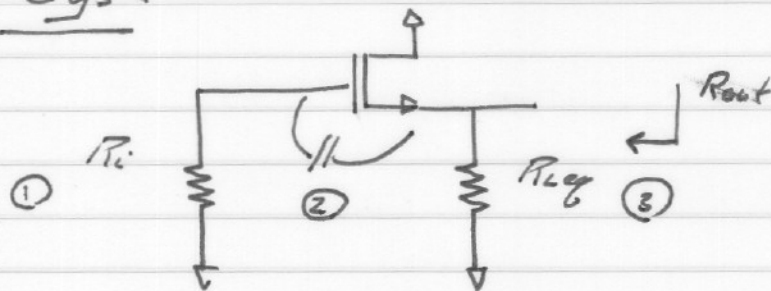
the capacitance  $C_{gd}$  sees resistance  $R_i$

$\Rightarrow$  Time constant of  $C_{gd} \cdot R_i$



the capacitance  $C_L$  sees resistance  $R_{eq} \parallel 1/g_m$

$\Rightarrow$  time constant of  $C_L (R_{eq} \parallel 1/g_m)$

$C_{gs}$ 

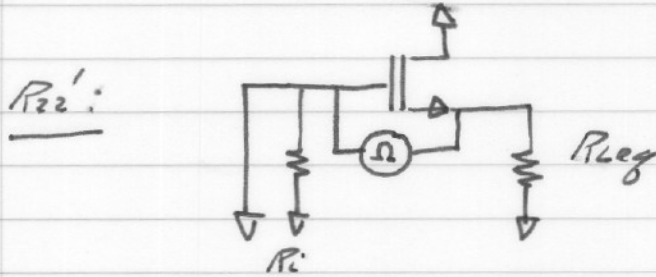
$$C_{gs} \cdot R_{22}^{\circ} = C_{gs} \left[ R_i (1 - A_v) + \overbrace{(\frac{1}{g_m}) \parallel R_{L_{eq}}}^{R_{out}} \right]$$

$$= C_{gs} \left[ R_i \left[ 1 - \frac{R_{L_{eq}}}{R_{L_{eq}} + \frac{1}{g_m}} \right] + (\frac{1}{g_m}) \parallel R_{L_{eq}} \right]$$

Now find  $a_2$

$$a_2 = R_{11}^0 C_1 C_2 R_{22}^1 + R_{11}^0 C_1 C_3 R_{33}^1 + R_{22}^3 C_2 C_3 R_{33}^0$$

$$R_{11}^0 = R_i, \quad R_{33}^0 = (1/g_m) \parallel R_{\text{sig}}$$



$$R_{22}^0 = R_i \left( 1 - \frac{\beta R_{\text{sig}}}{R_{\text{sig}} + 1/g_m} \right) + \frac{1}{g_m} \parallel R_{\text{sig}}$$

$$R_{22}^1 = 0 \left( 1 - \frac{\beta R_{\text{sig}}}{R_{\text{sig}} + 1/g_m} \right) + \frac{1}{g_m} \parallel R_{\text{sig}}$$

$$= (1/g_m) \parallel R_{\text{sig}}$$

$$R_{33}^1 = \text{expression for } R_{33}^0 \text{ except with } R_i \rightarrow 0$$

$$= (1/g_m) \parallel R_{\text{sig}}$$

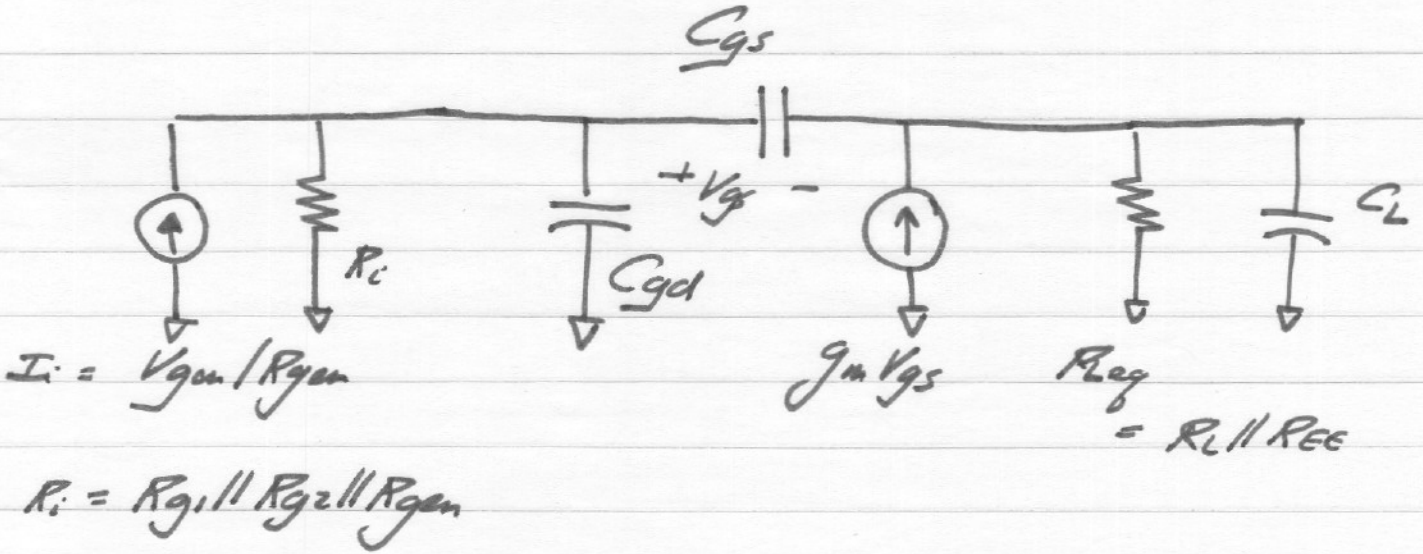
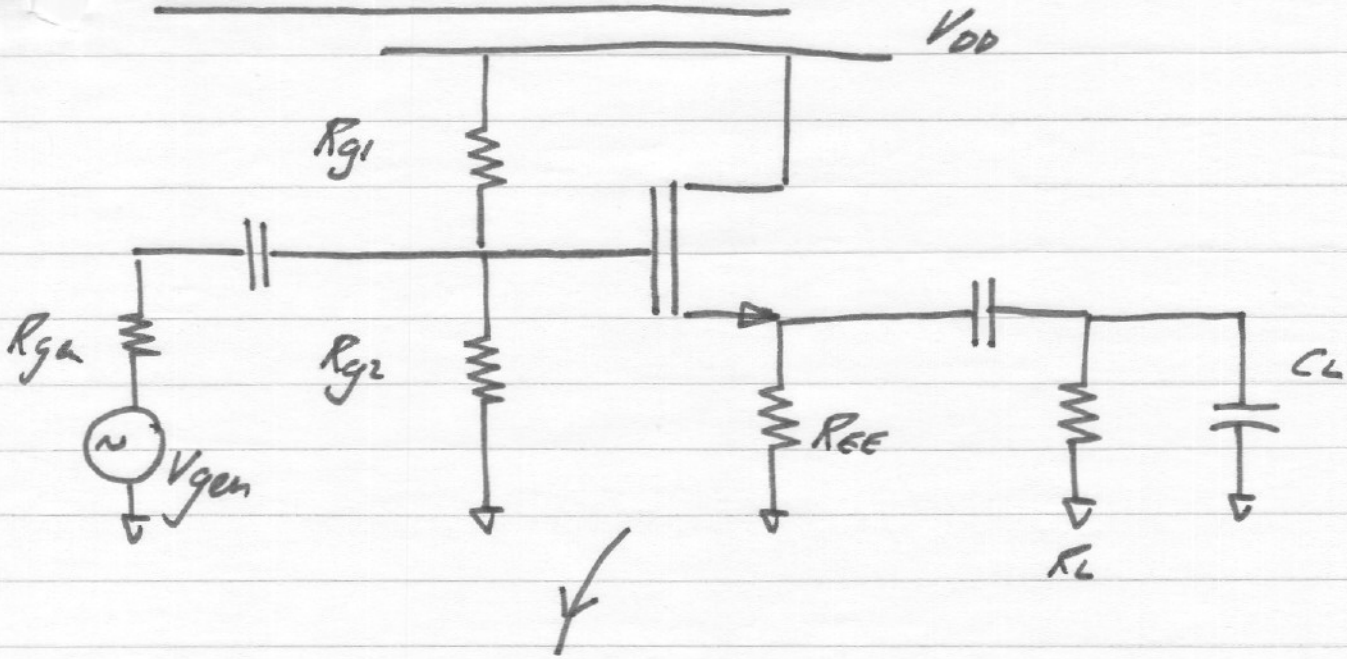
$$R_{22}^3 = \text{expression for } R_{22}^0 \text{ except with } R_{\text{sig}} = 0$$

$$= R_i$$

$$a_2 = R_i \cdot \left[ \frac{1}{g_m} \parallel R_{\text{sig}} \right] \left[ C_{gs} C_{gd} + C_{gs} C_c + C_{gd} C_c \right]$$



MOSFET Source Follower



we can, once again, apply exactly the same

same methods as for the bjt case.

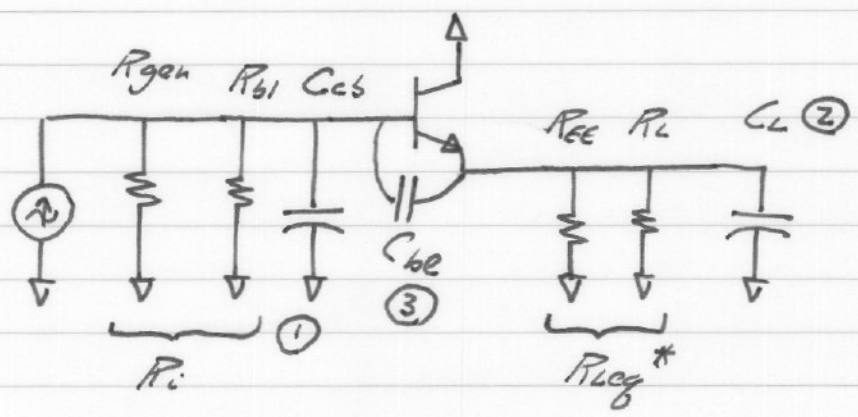
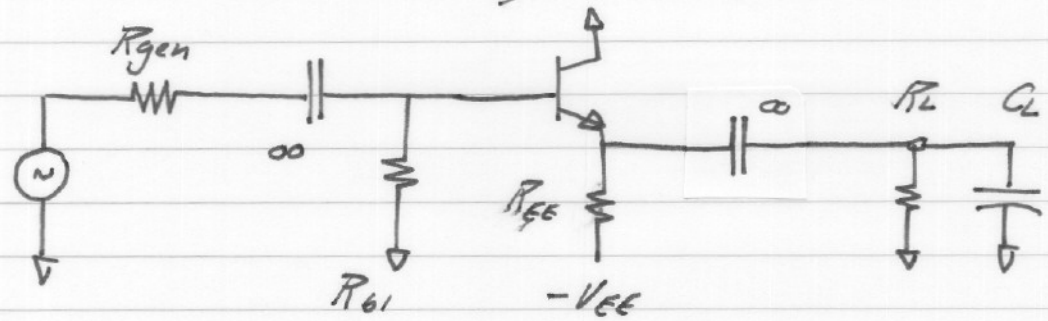
106

$$v_o / v_{gen} = \frac{v_o}{v_{gen}} \bigg|_{MB} \frac{1 + b_1 s}{1 + a_1 s + a_2 s^2}$$

$$b_1 = \text{by other methods} = C_{gs} / g_m$$

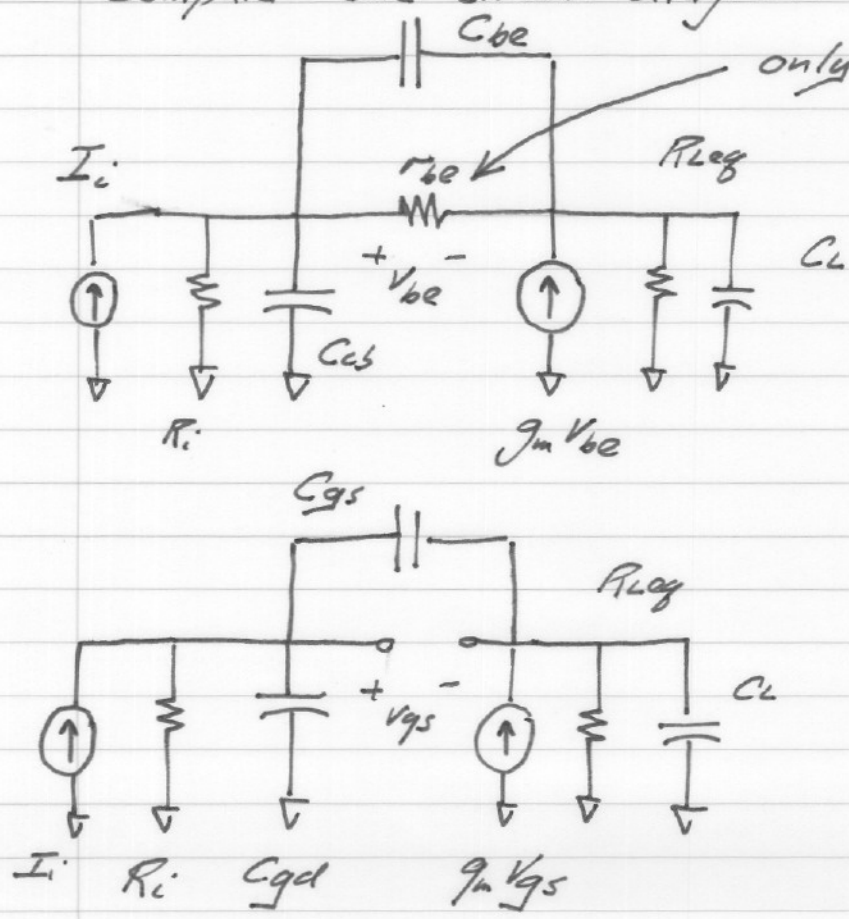
$$a_1 = C_{gd} \cdot R_i + C_L (R_L \parallel 1/g_m) \\ + C_{gs} [ (1/g_m) \parallel R_{eq} + R_i (1 - A_v) ]$$

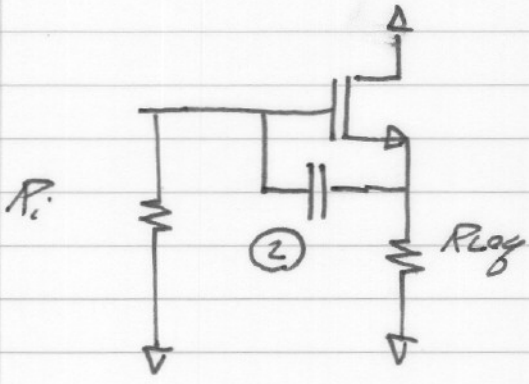
Emitter follower by MOTC



\* includes REE

Compare the circuit diagrams of  $-1\beta$  &  $-1/g_m$  followers



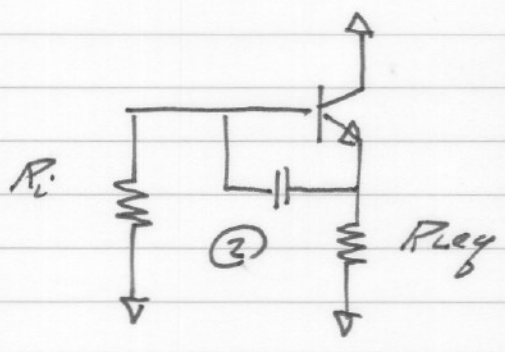


Given that for the MOSFET

$$R_{22}^0 C_{gs} = C_{gs} \left[ \left( 1 - \frac{R_{leg}}{R_{leg} + 1/g_m} \right) R_i + \frac{1}{g_m} \parallel R_{leg} \right]$$

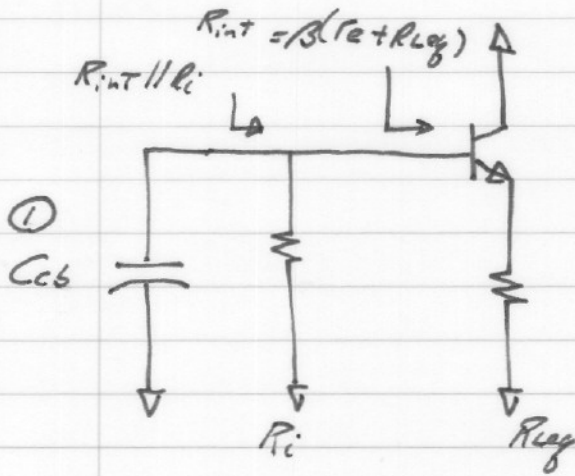
We have simply added  $R_{\pi} = \beta / g_m$

in parallel:

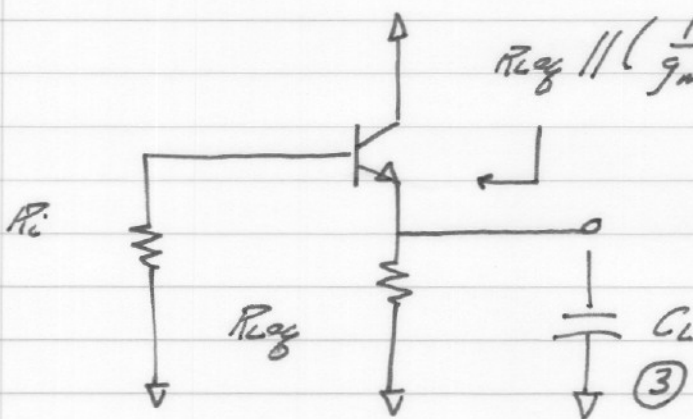


$$R_{22}^0 = \left[ R_i \left( 1 - \frac{R_{leg}}{R_{leg} + 1/g_m} \right) + \frac{1}{g_m} \parallel R_{leg} \right] \parallel \frac{\beta}{g_m}$$

The other time constants for the e.f. are simple:



$$R_{11}^0 = R_i \parallel \beta(r_e + R_{ce})$$



$$R_{33}^0 = R_{ce} \parallel \left( \frac{1}{g_m} + \frac{R_i}{\beta} \right)$$

So the overall EF transfer function is:

$$\frac{V_o}{V_{gen}} = \frac{V_o}{V_{gen}} \bigg|_{MS} \frac{1 + b_1 A}{1 + a_1 A + a_2 A^2}$$

$$a_1 = C_{cb} \cdot R_i \parallel R_{inT}$$

$$R_{inT} = \beta (r_e + R_{eq})$$

$$+ C_{be} \cdot \left\{ R_{be} \parallel \left\{ R_i (1 - A_v) + R_{eq} \parallel \frac{1}{g_m} \right\} \right\}$$

$$+ C_L \cdot R_{eq} \parallel \left( \frac{1}{g_m} + R_i / \beta \right)$$

$$a_2 = (R_i \parallel R_{inT}) \left( \frac{1}{g_m} \parallel R_{eq} \right)$$

$$\times [ C_{cb} C_{be} + C_{cb} C_L + C_{be} C_L ]$$

Source follower example:

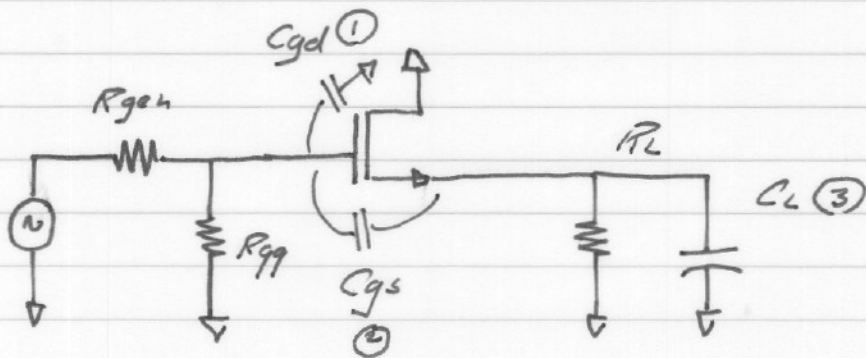
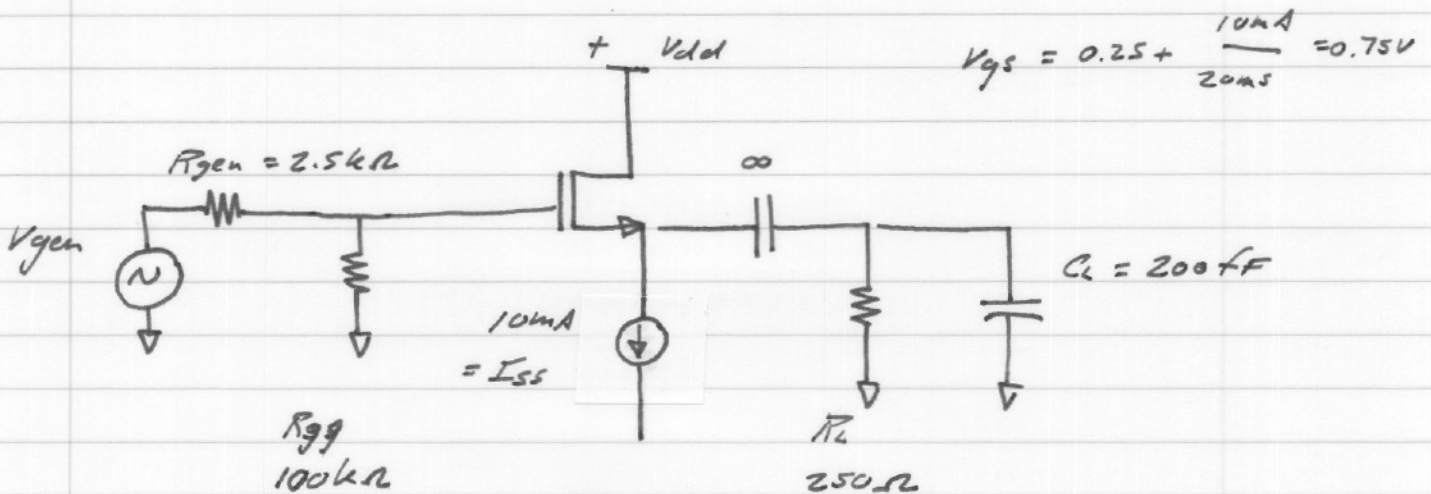
MOSFET :  $C_{ox} \mu_{sat} = 1 \text{ mS}/\mu\text{m}$   $V_{th} = 0.25 \text{ V}$

$\lambda = 0$  (simplify)  $W_g = 20 \mu\text{m}$   $L_g = 200 \text{ nm}$   $\mu_{sat} = 10^7 \text{ cm}^2/\text{s}$

$\Rightarrow C_{gs} = C_{ox} \cdot L_g \cdot W_g = \frac{1 \text{ mS}/\mu\text{m}}{10^5 \text{ m/s}} \cdot 200 \text{ nm} \cdot 20 \mu\text{m} = 40 \text{ fF}$

$g_m = 1 \text{ mS}/\mu\text{m} \times 20 \mu\text{m} = 20 \text{ mS}$  ( $f_T = 79.5 \text{ GHz}$ )

lets assume  $C_{gd} = 0.1 C_{gs} = 4 \text{ fF}$



Mid-band analysis

$$R_{\text{sig}} = 250 \Omega \quad A_{\text{vms}} = \frac{250}{250 \Omega + \underbrace{1/20 \text{ms}}_{50 \Omega}} = 0.8333$$

$$v_m/v_{\text{gen}} = 0.976 \quad v_o/v_{\text{gen}} = 0.813$$

$$R_i = R_{\text{gen}} \parallel R_{\text{gg}} = 2.44 \text{ k}\Omega$$

$$R_{\text{sig}} \parallel 1/g_m = 49 \Omega$$

High Frequency Analysis

$$R_{11} \circ C_{\text{gd}} = 2.44 \text{ k}\Omega \cdot 4 \text{ fF} = 9.8 \text{ ps}$$

$$R_{32} \circ C_L = 49 \Omega \cdot 200 \text{ fF} = 9.8 \text{ ps}$$

$$C_{\text{gs}} \cdot R_{22} = 40 \text{ fF} [2.44 \text{ k}\Omega \cdot (1 - 0.8333) + 49 \Omega]$$

$$= 40 \text{ fF} [456 \Omega] = 18.2 \text{ ps}$$

$$a_1 = 37.8 \text{ ps}$$

$$a_2 = 2.44 \text{ k}\Omega \cdot 49 \Omega \cdot [4 \text{ fF} \cdot 200 \text{ fF} + 4 \text{ fF} \cdot 40 \text{ fF} + 40 \text{ fF} \cdot 200 \text{ fF}]$$

$$= 1.07 (10^{-21}) \text{ sec}^2 = (32.7 \text{ ps})^2$$



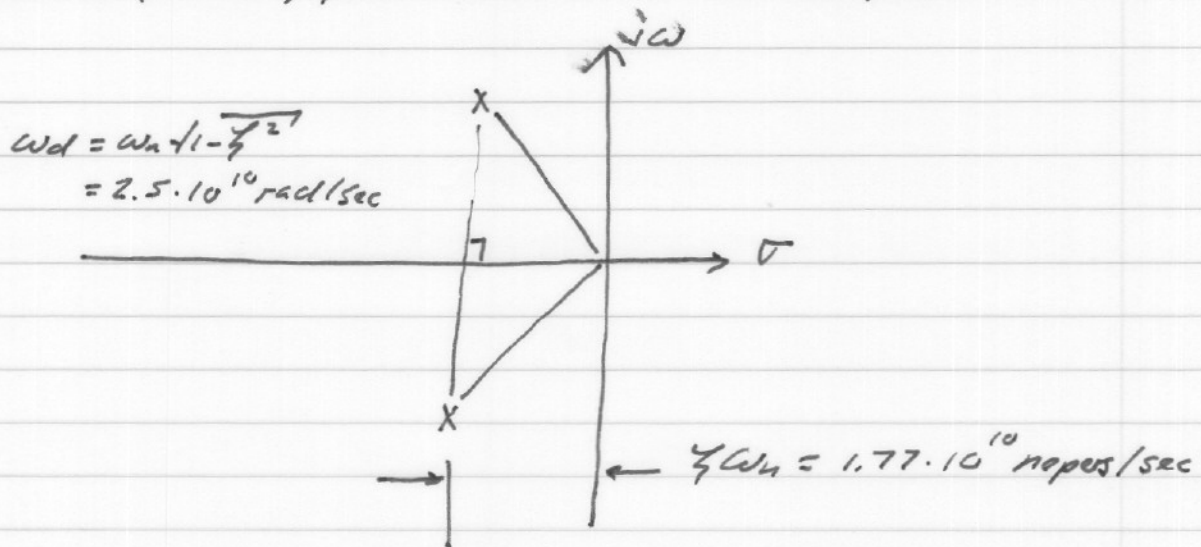
The ratio of  $a_2/a_1^2$  is such that the SPA is not valid. See if the poles are complex

$$1 + a_1 A + a_2 A^2 = 1 + (2\zeta/\omega_n)A + A^2/\omega_n^2$$

$$\omega_n = 1/\sqrt{a_2} = 3.06 \cdot 10^{10} \text{ rad/sec}; \quad \underline{f_n = 4.9 \text{ GHz}}$$

$$\zeta = a_1 / 2\sqrt{a_2} = 0.58$$

Since  $\zeta < 1$ , poles are indeed complex.



the transfer function also has a zero at

$$f_z = (1/2\pi) \text{ gm/Cgs} \approx f_T = 80 \text{ GHz}$$

