

InGaAs/InP DHBTs with Emitter and Base Defined through Electron-beam Lithography for Reduced C_{cb} and Increased RF Cut-off Frequency

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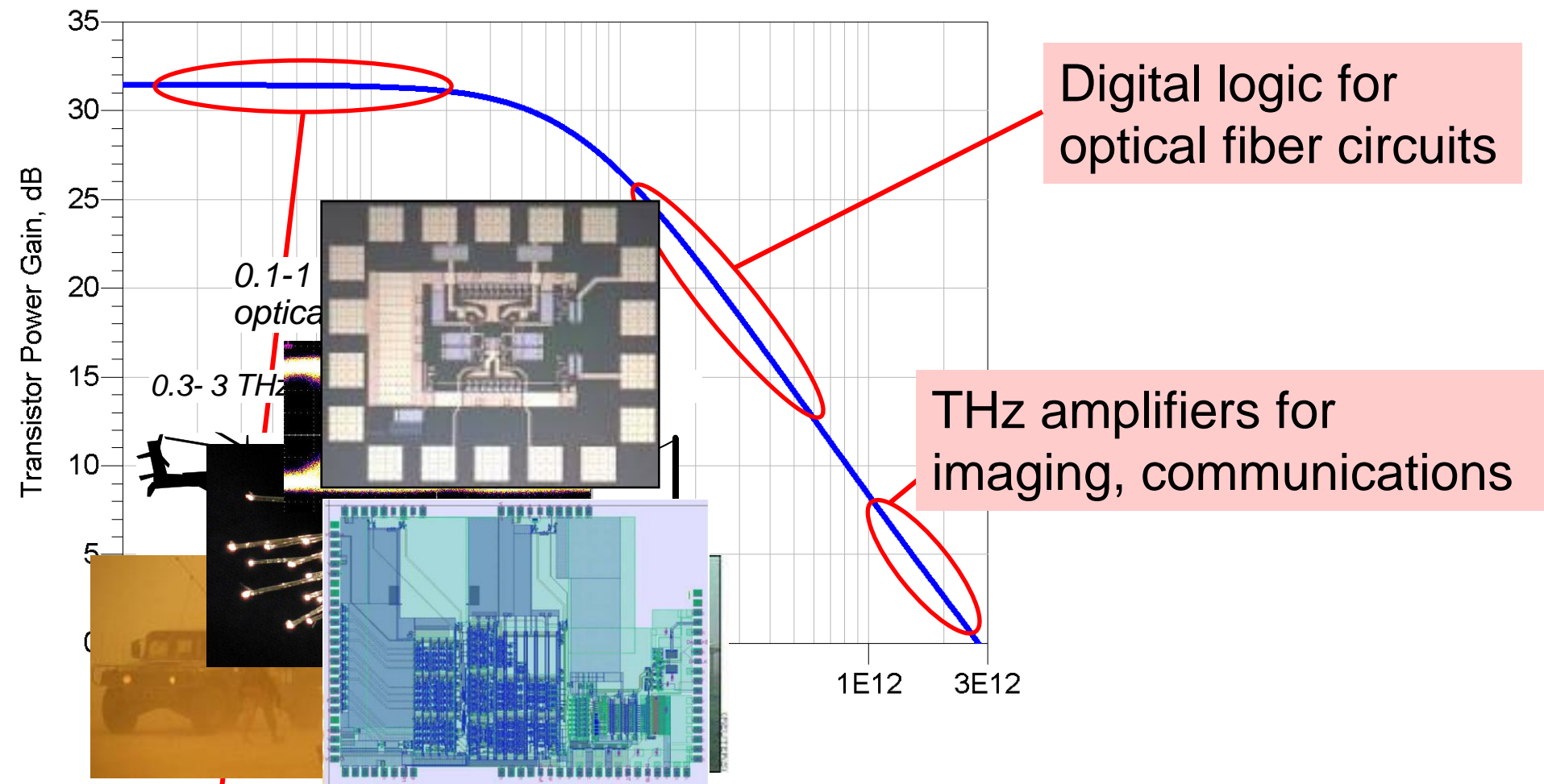
Agilent Technologies



Outline

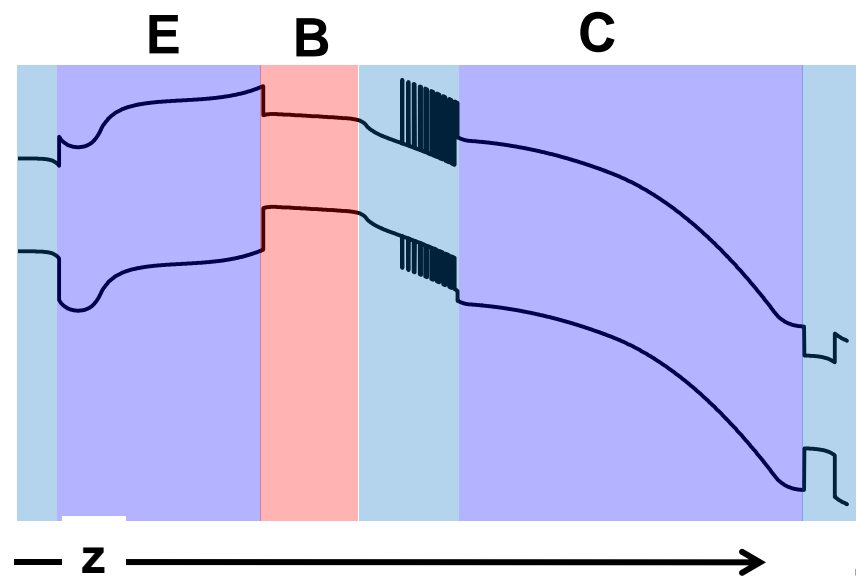
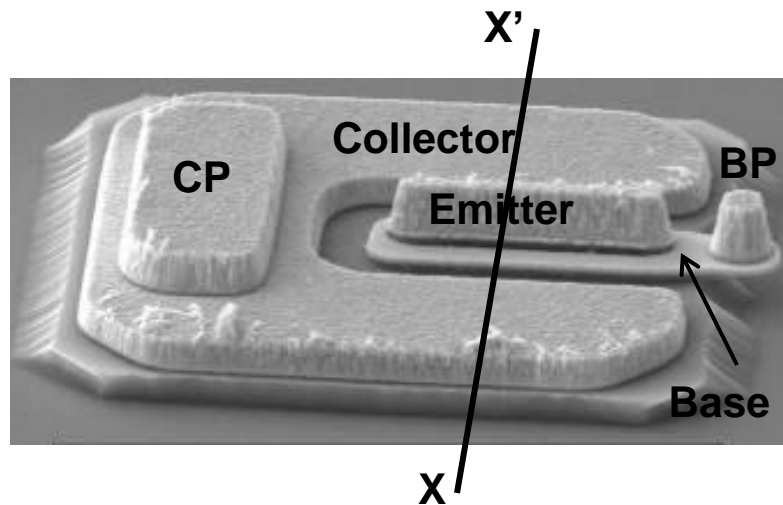
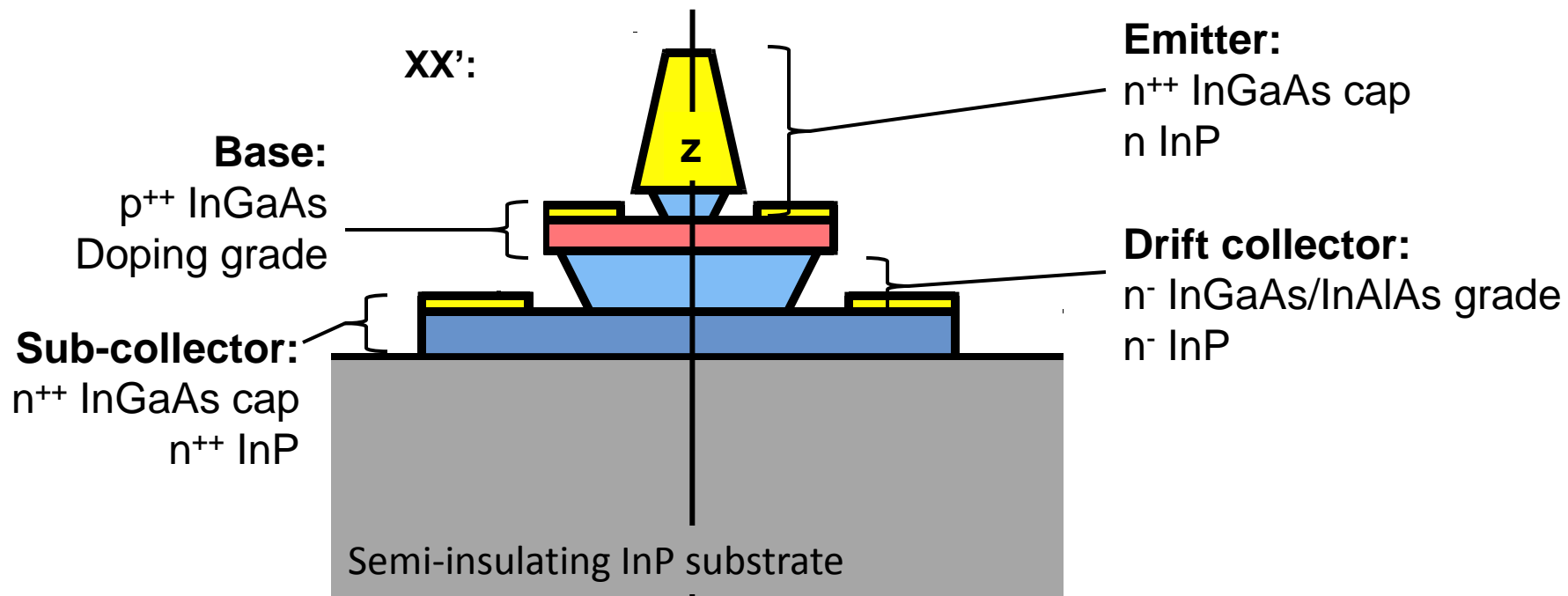
- Motivation
- HBT Design & Scaling
- Fabrication Process & Challenge
- Electrical Measurements
- Conclusion

Why THz Transistors?



High gain at microwave frequencies:
Precision analog design, high resolution ADCs, DACs

Type-I InP DHBTs at UCSB

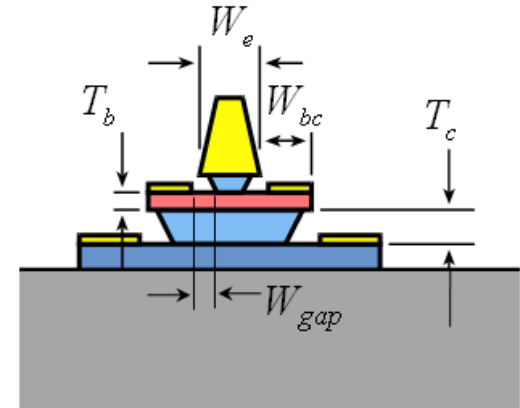


HBT Scaling Laws

To double bandwidth of a mesa DHBT:

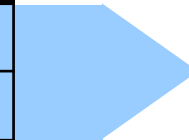
Keep **constant** all **resistances** and **currents**

Reduce 2:1 all **capacitances** and **transport delays**

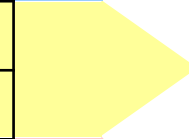


(emitter length L_e)

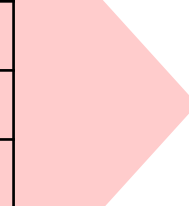
Parameter	Change
collector depletion layer thickness	decrease 2:1
base thickness	decrease 1.41:1
emitter junction width	decrease 4:1
collector junction width	decrease 4:1
emitter contact resistivity	decrease 4:1
base contact resistivity	decrease 4:1
current density	increase 4:1



Epitaxial scaling



Lateral scaling

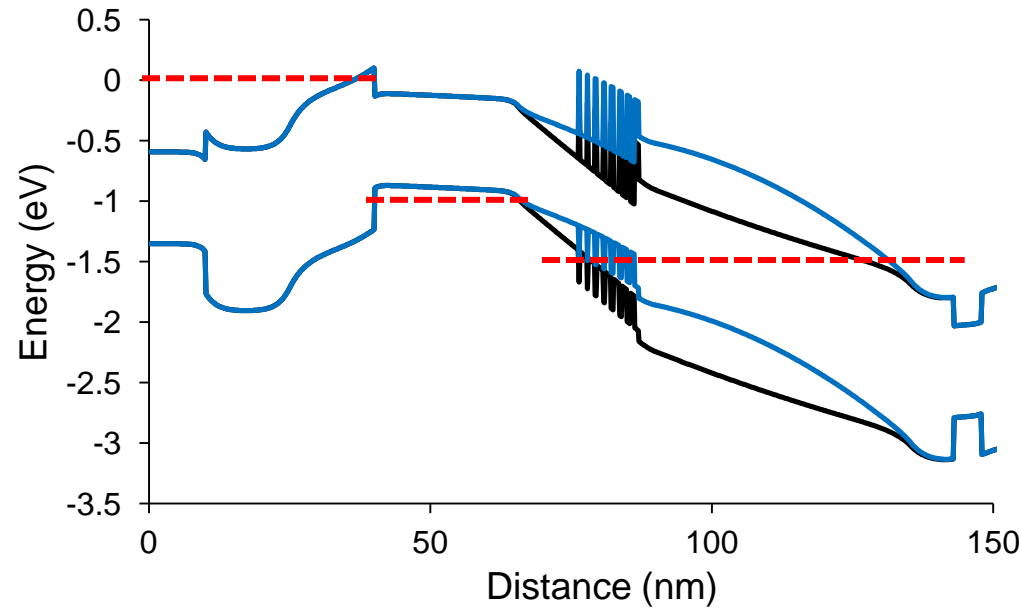


**Surface prep
& doping**

Keep lengths the same, reduce widths 4:1 for thermal considerations

Epitaxial Design

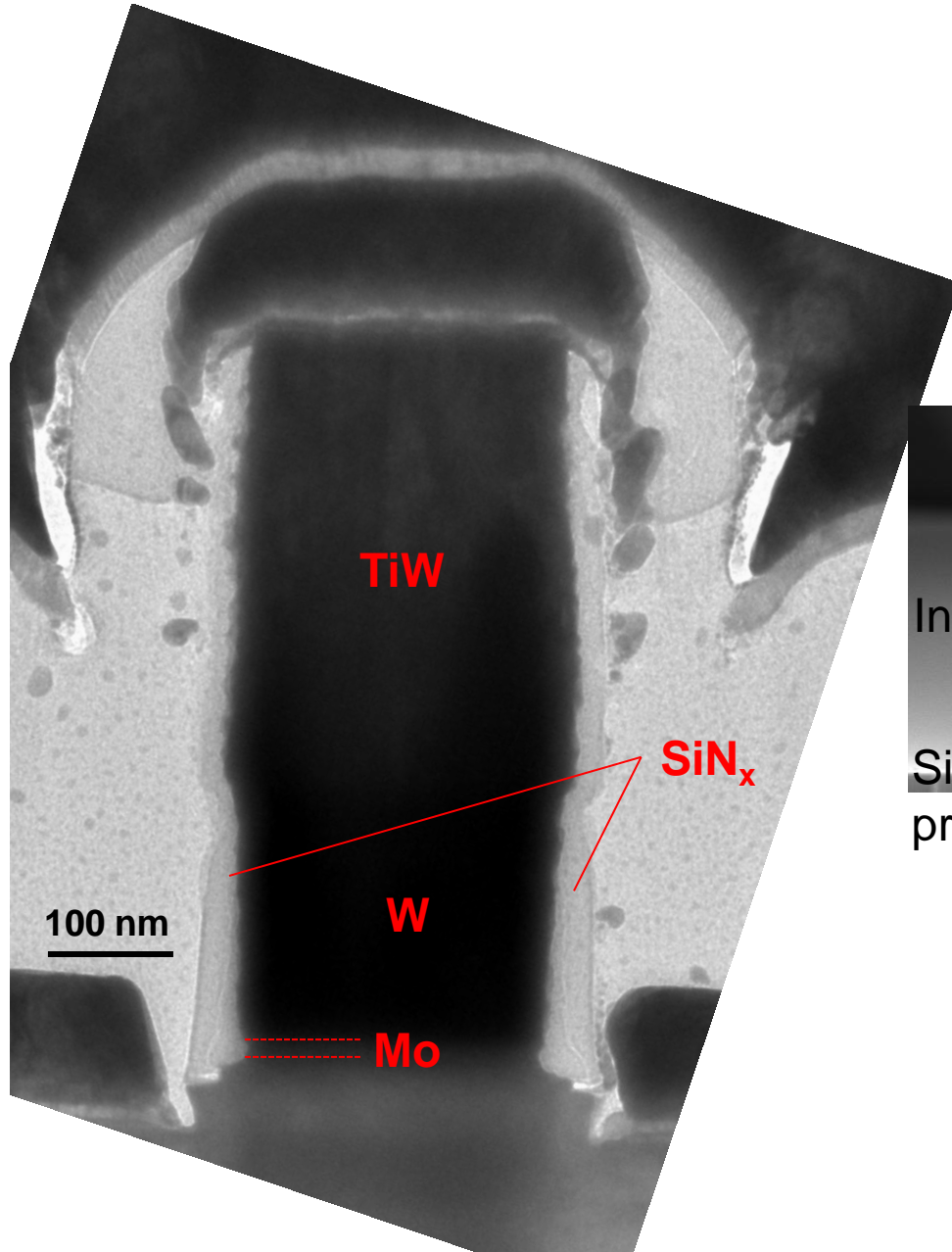
T(nm)	Material	Doping (cm ⁻³)	Description
10	In _{0.53} Ga _{0.47} As	8·10 ¹⁹ : Si	Emitter cap
15	InP	5·10 ¹⁹ : Si	Emitter
15	InP	2·10 ¹⁸ : Si	Emitter
25	InGaAs	1-0.5·10 ²⁰ : C	Base
9.5	In _{0.53} Ga _{0.47} As	1·10 ¹⁷ : Si	Setback
12	InGaAs / InAlAs	1·10 ¹⁷ : Si	B-C Grade
3	InP	5·10 ¹⁸ : Si	Pulse doping
45.5	InP	1·10 ¹⁷ : Si	Collector
7.5	InP	1·10 ¹⁹ : Si	Sub Collector
5	In _{0.53} Ga _{0.47} As	4·10 ¹⁹ : Si	Sub Collector
300	InP	1·10 ¹⁹ : Si	Sub Collector
3.5	In _{0.53} Ga _{0.47} As	Undoped	Etch stop
Substrate	SI : InP		



$$V_{be} = 1.0V, V_{cb} = 0.5V, J_e = 0, 27 \text{ mA}/\mu\text{m}^2$$

Thin (**70 nm**) collector for **balanced** f_T/f_{max}
 High emitter/base doping for low R_{ex}/R_{bb}

Sub-200 nm Emitter Anatomy



Hybrid sputtered metal stack for low-stress, vertical profile

W/TiW interfacial discontinuity enables base contact lift-off

High-stress emitters fall off

Very thin emitter epitaxial layer for minimal undercut



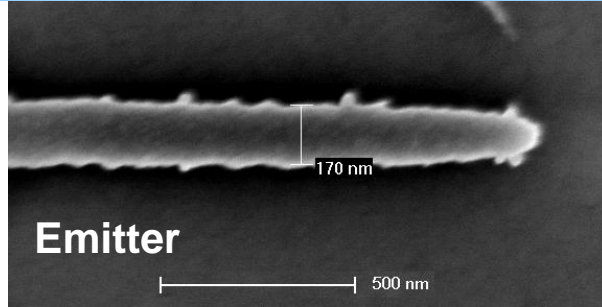
Semiconductor wet etch
Interfacial Mo blanket-evaporated for low ρ_c
undercuts emitter contact

SiN_x sidewalls protect emitter contact, prevent emitter base shorts

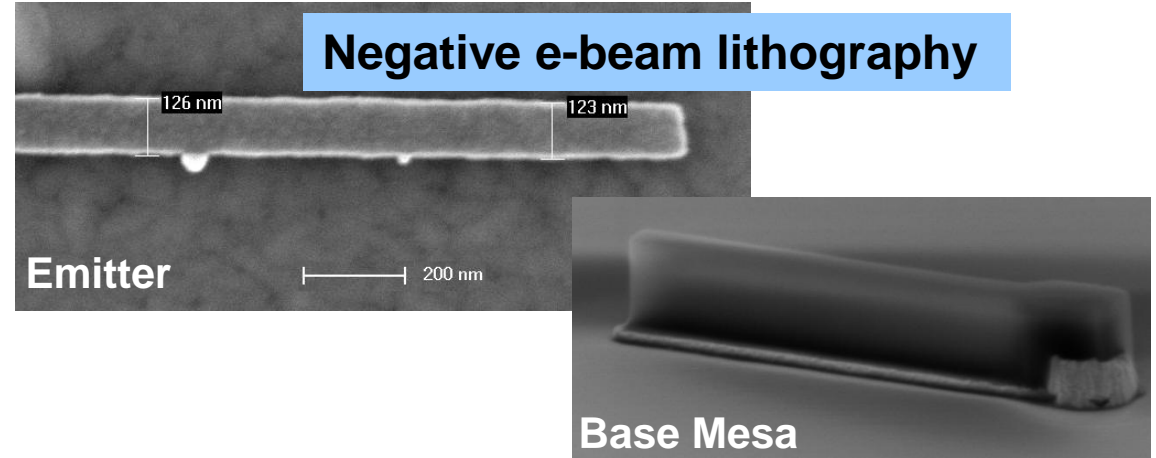
Single sputtered metal has non-vertical etch profile

Lithographic Scaling and Alignment

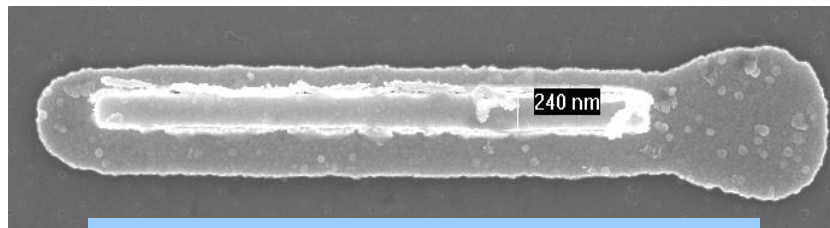
Positive i-line lithography



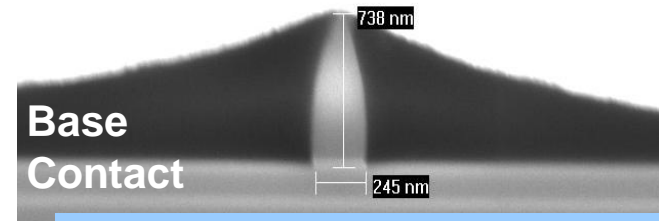
Negative e-beam lithography



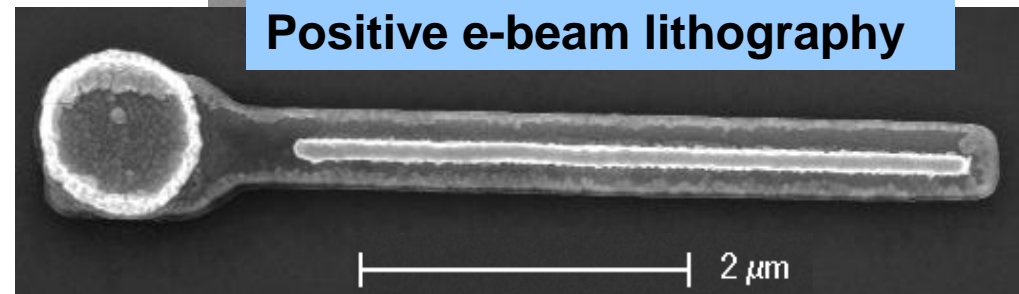
E-beam lithography needed to define < 150 nm emitters and for < 50 nm emitter-base contact misalignment

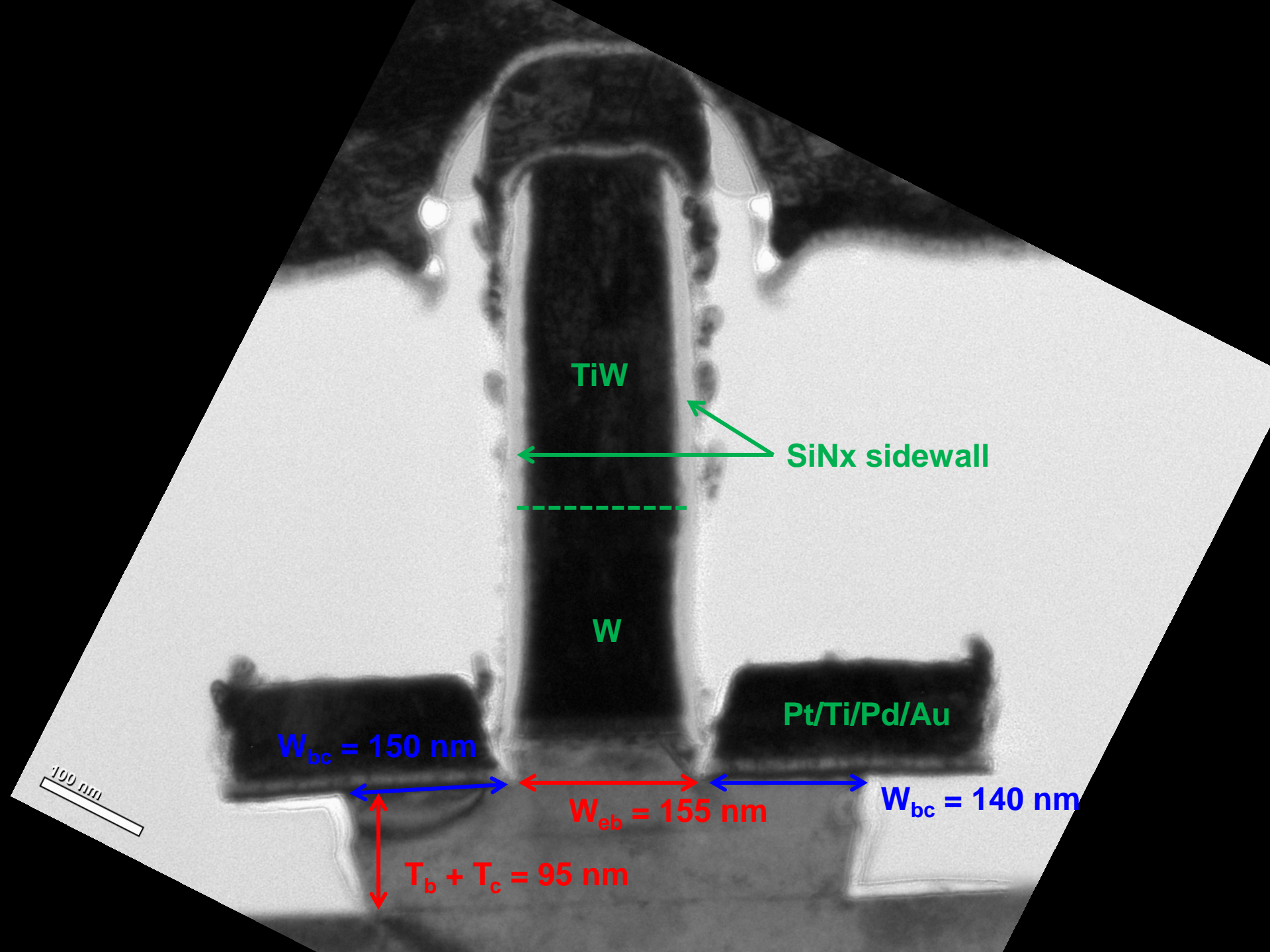


Negative i-line lithography



Positive e-beam lithography





TiW

SiNx sidewall

W

Pt/Ti/Pd/Au

$W_{bc} = 150 \text{ nm}$

$W_{cb} = 155 \text{ nm}$

$W_{bc} = 140 \text{ nm}$

$T_b + T_c = 95 \text{ nm}$

100 nm

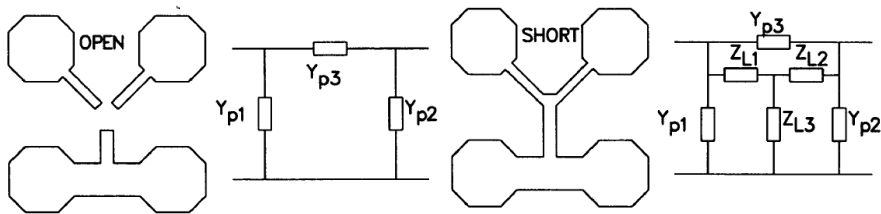
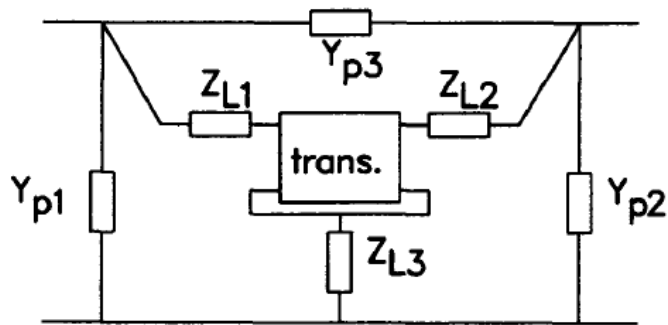
Measurement

RF measurements conducted using Agilent E8361A PNA from 1-67 GHz

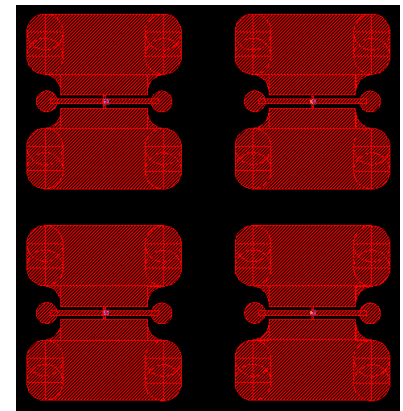
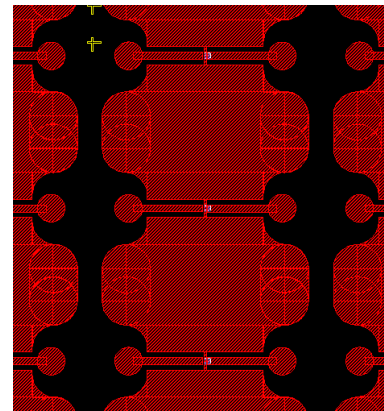
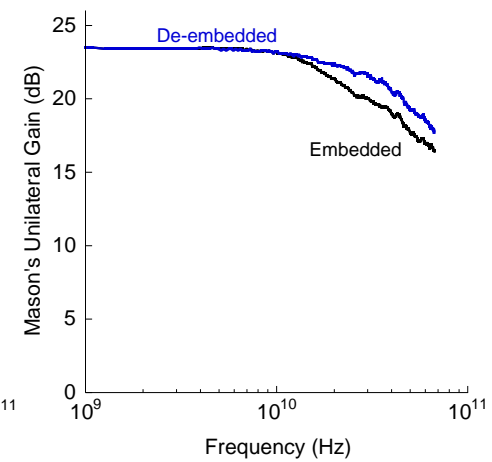
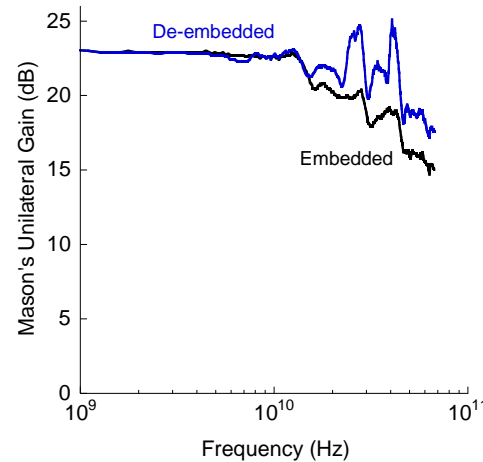
DC bias and measurements made with Agilent 4155 SPA

Off-wafer LRRM calibration, lumped-element pad stripping used to de-embed device S-Parameters

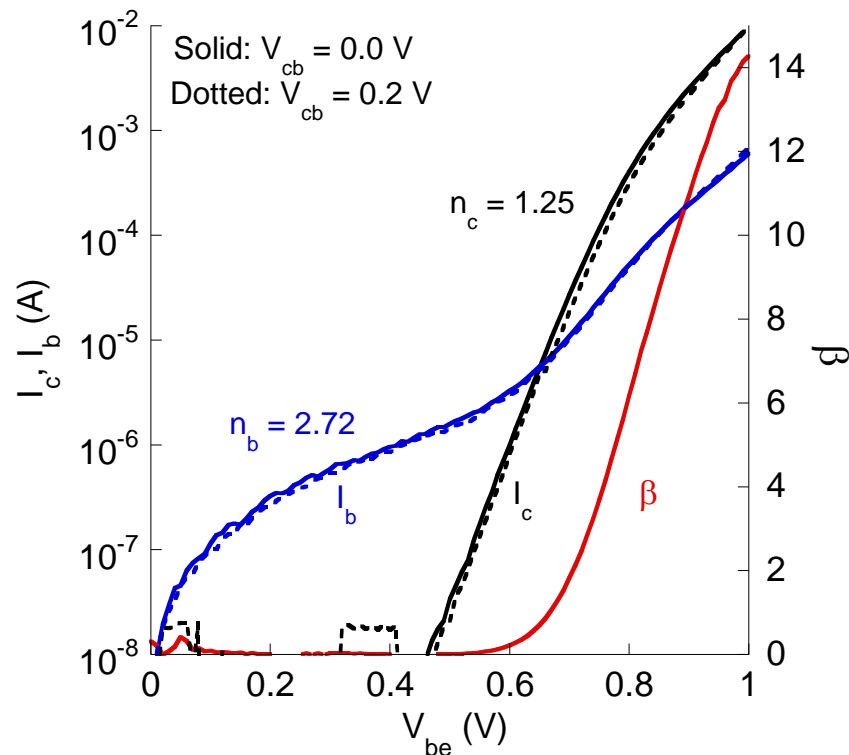
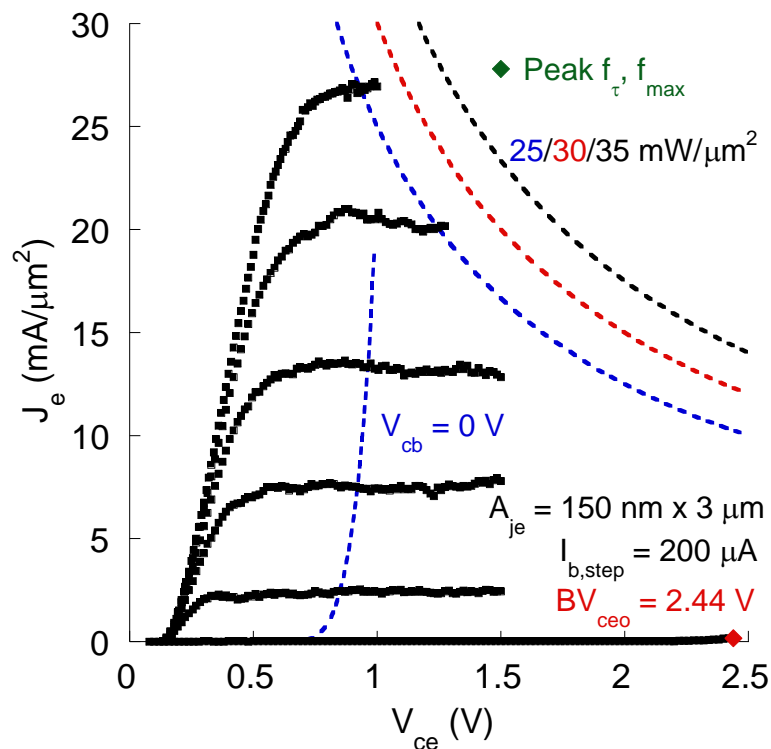
Isolated pad structures used to provide clean RF measurements



$$Y_{trans} = ((Y_{dut} - Y_{open})^{-1} - (Y_{short} - Y_{open})^{-1})^{-1}$$



DC Data



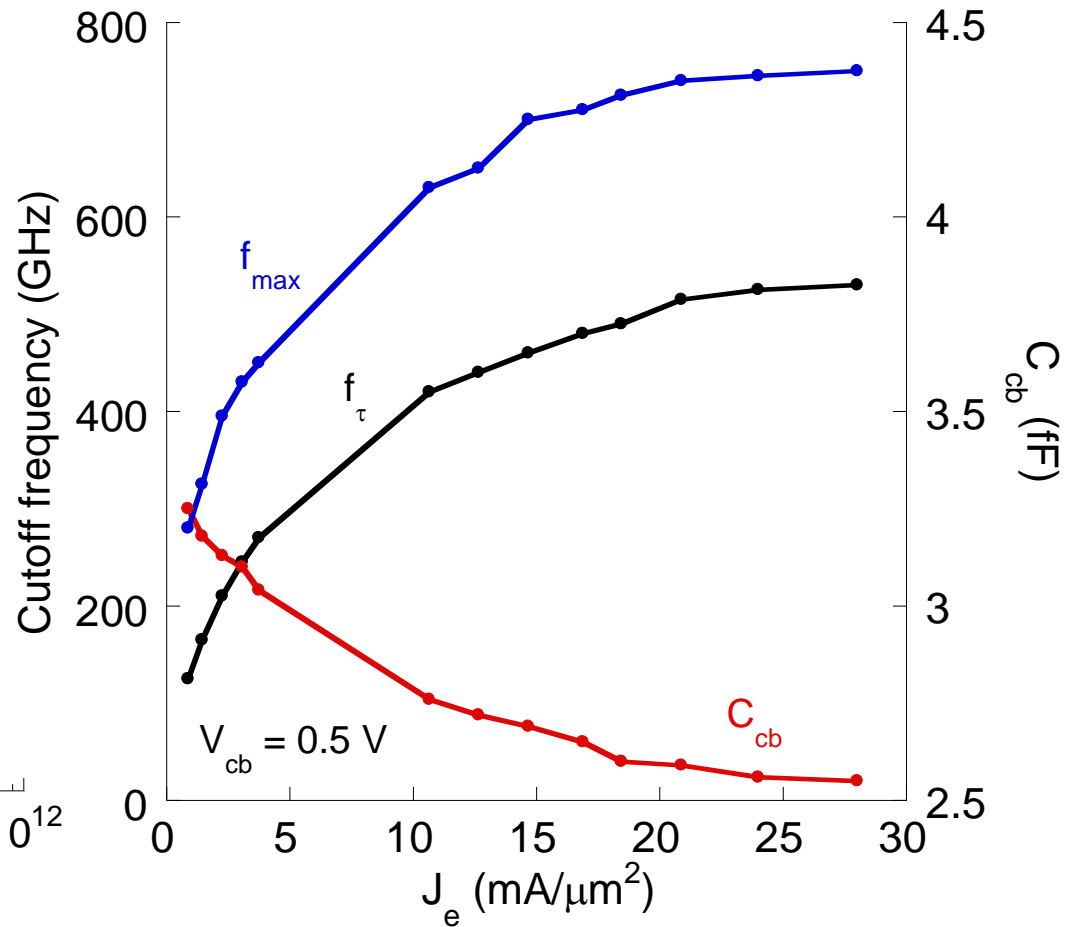
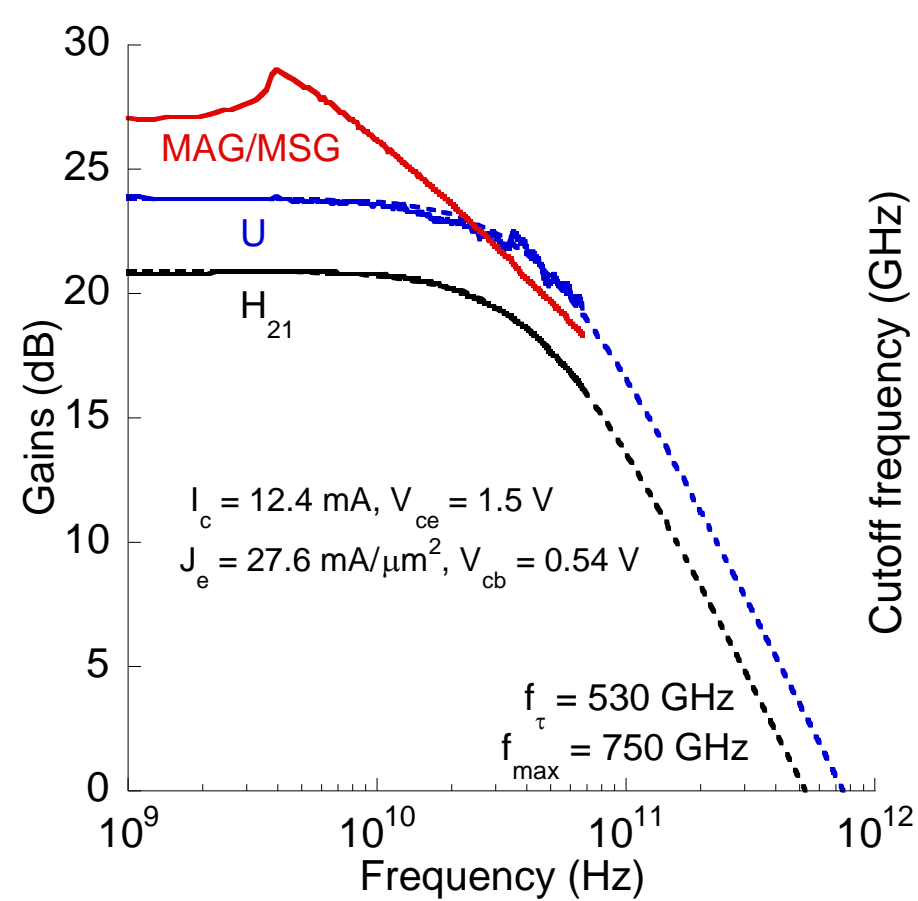
$\beta = 14$ for 150 nm junction

$V_{B_{ceo}} = 2.44 \text{ V}$ @ $J_e = 15 \text{ kA/cm}^2$

$R_{ex} \approx 2 \Omega \cdot \mu\text{m}^2$ (RF extraction)

Collector $\rho_{sheet} = 14 \Omega/\square$, $\rho_c = 12 \Omega \cdot \mu\text{m}^2$

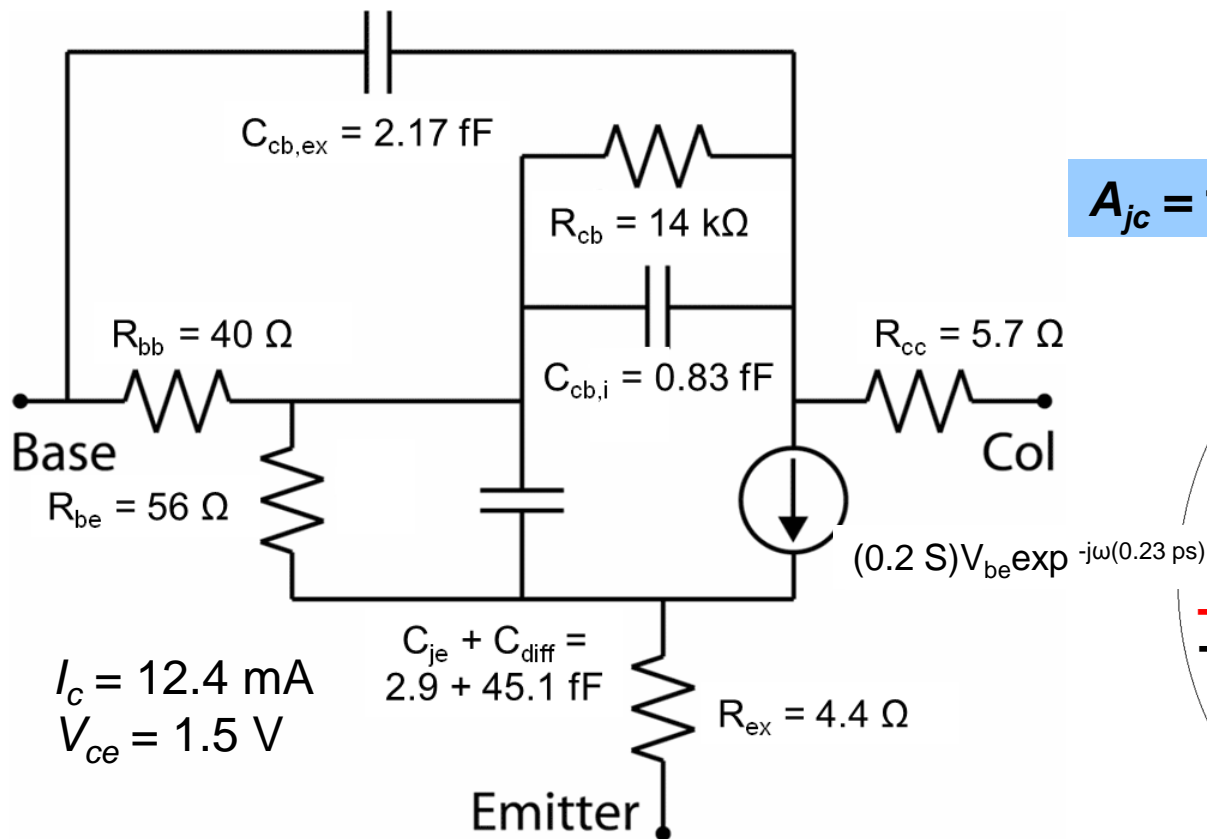
RF Data



Peak **RF performance at >40 mW/ μm^2**

Kirk limit not reached

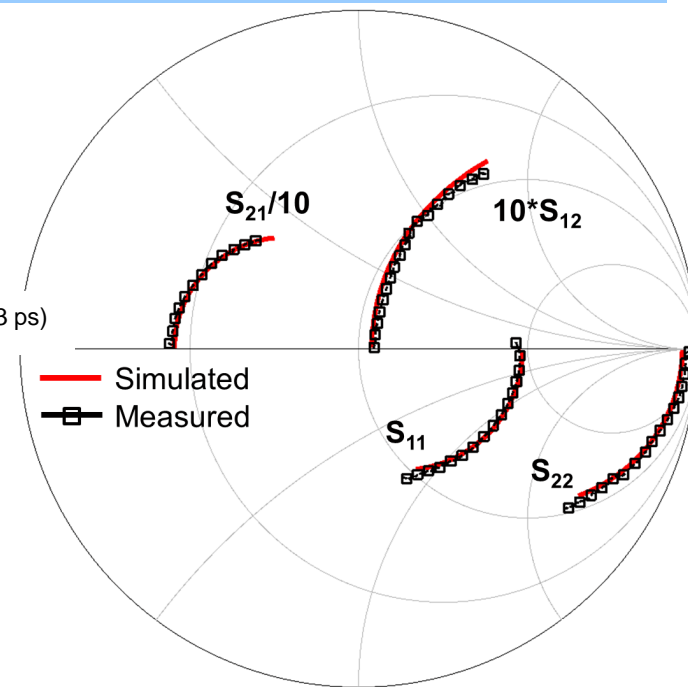
Equivalent Circuit Model



$$\rho_{ex} = 2 \Omega \cdot \mu\text{m}^2$$

$$C_{cb} = 3.0 \text{ fF}$$

$$A_{jc} = 1.86 \mu\text{m}^2 \sim 450 \text{ nm} \times 4 \mu\text{m}$$



Lowest ρ_{ex} to date due to Mo contact, highly doped epi

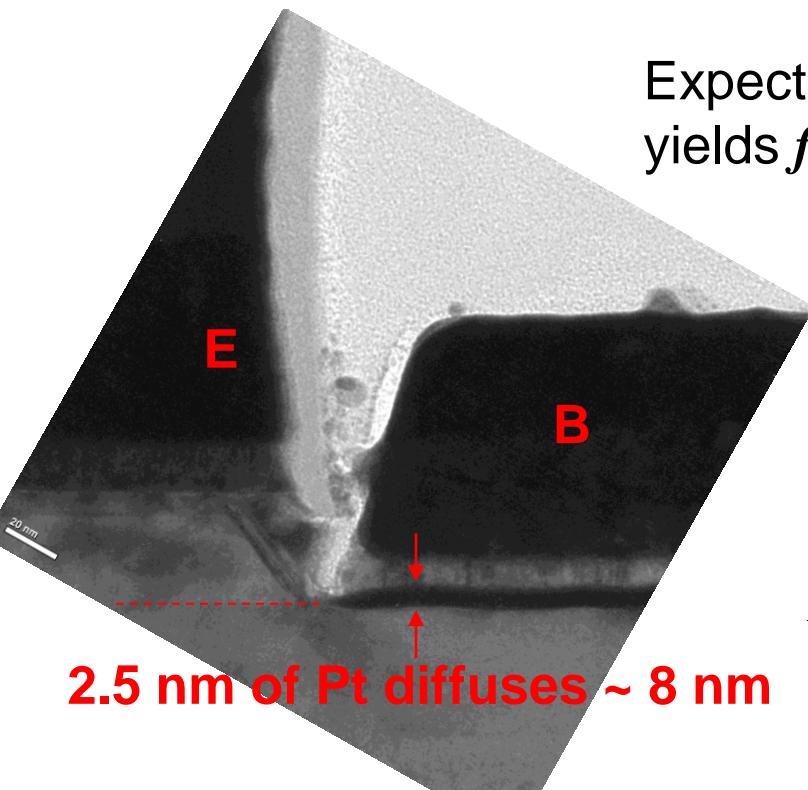
C_{cb} lower than 100 nm collector epi designs due to E-beam litho

Performance Analysis

$$\frac{1}{2\pi f_\tau} = \underbrace{\tau_b + \tau_c}_{230 \text{ fs}} + \underbrace{\frac{nk_B T}{qI_c} C_{je}}_{15 \text{ fs}} + \underbrace{\left(\frac{nk_B T}{qI_c} + R_{ex} + R_c \right) C_{cb}}_{45 \text{ fs}}$$

τ_{ec} dominated by **transit delays**, high **ideality factor** reduces $f_\tau \sim 10\%$

Expected base $\rho_c = 4 \Omega \cdot \mu\text{m}^2$ and $R_{sh} = 800 \Omega/\square$ yields $f_{max} > 1.0 \text{ THz}$ for same f_τ



2.5 nm of Pt diffuses $\sim 8 \text{ nm}$

Epitaxial design, process damage explain high η_b, R_{bb}

R_{sh} increased by **base contacts reacting** with 5 nm (20 %) of base

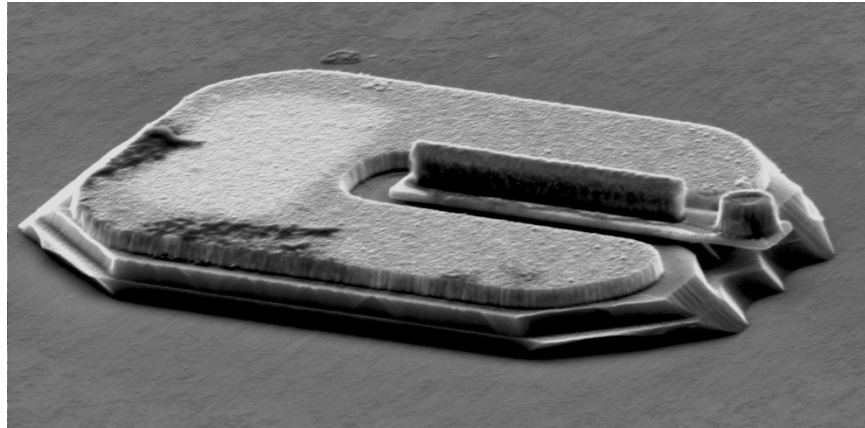
Conclusion

E-beam lithography used to define narrow emitter, ***narrowest base mesa*** reported to date

Narrow mesa, low emitter ρ_c enable 33% increase in f_{max} from previous UCSB results with 70 nm collector thickness

Epitaxial thinning increased f_T by 10% from 100 nm UCSB designs

1 THz bandwidth possible with improved base contact process



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Questions?

Extra Slides

Bipolar Scaling Laws

$$\tau_b \approx T_b^2 / 2D_n$$

$$\tau_c = T_c / 2v_{sat}$$

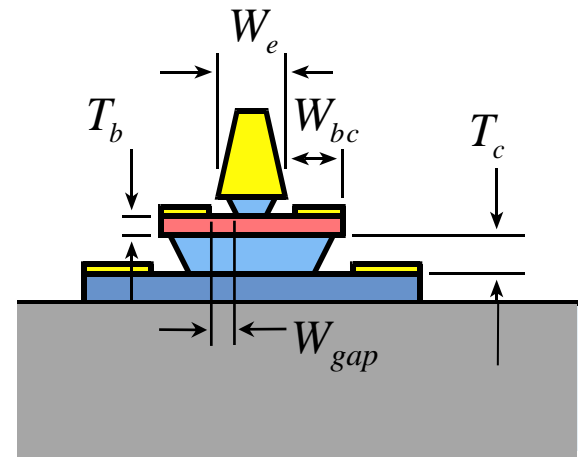
$$C_{cb} = \epsilon A_c / T_c$$

$$I_{c,max} \propto v_{sat} A_e (V_{cb} + V_{bi}) / T_c^2$$

$$\Delta T \propto \frac{P}{L_e} \left[1 + \ln \left(\frac{L_e}{W_e} \right) \right]$$

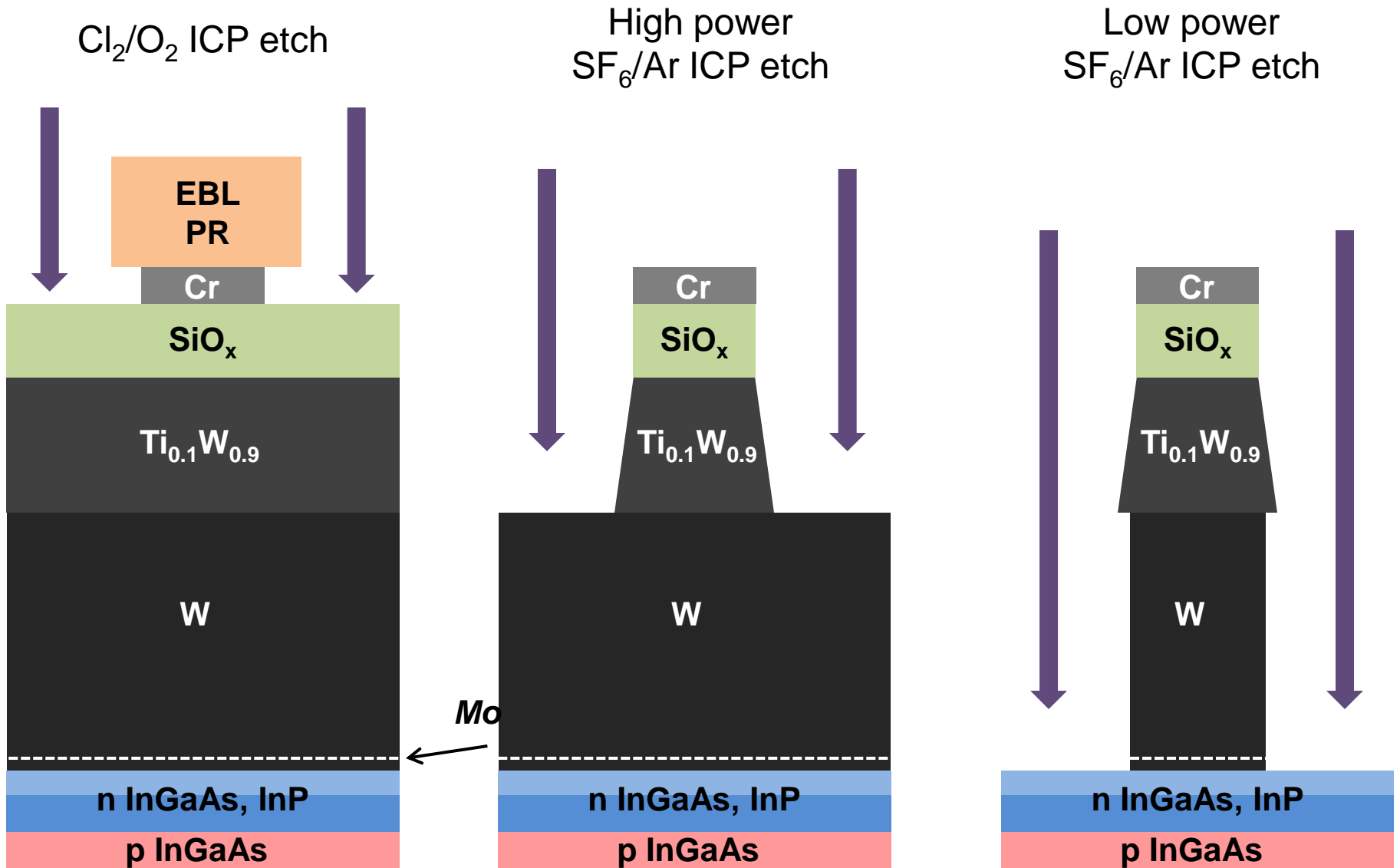
$$R_{ex} = \rho_{c,e} / A_e$$

$$R_{bb} = \frac{\rho_{sh}}{L_e} \left(\frac{W_{bc}}{6} + \frac{W_{gap}}{2} + \frac{W_e}{12} \right) + \frac{\rho_{c,b}}{A_{c,b}}$$



(emitter length L_e)

Fabrication: Emitter contact

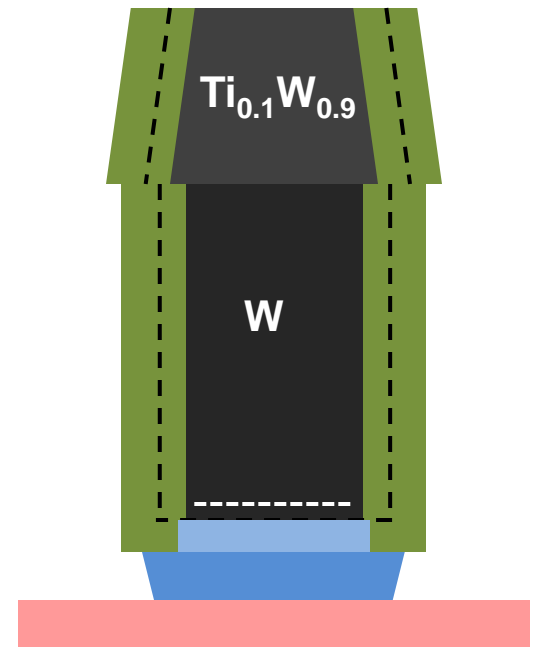
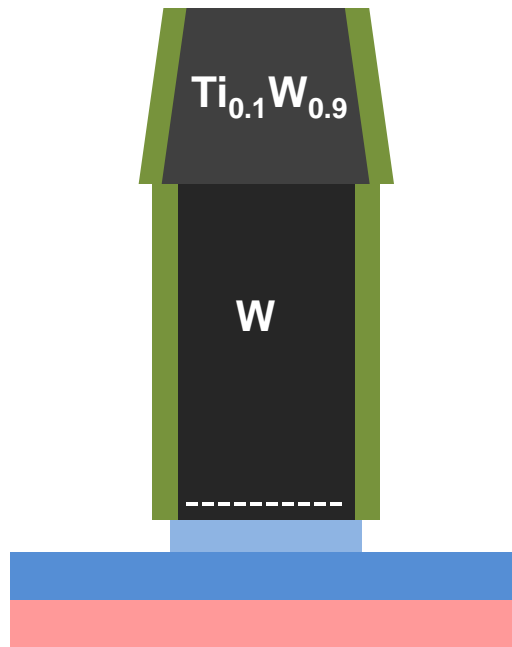
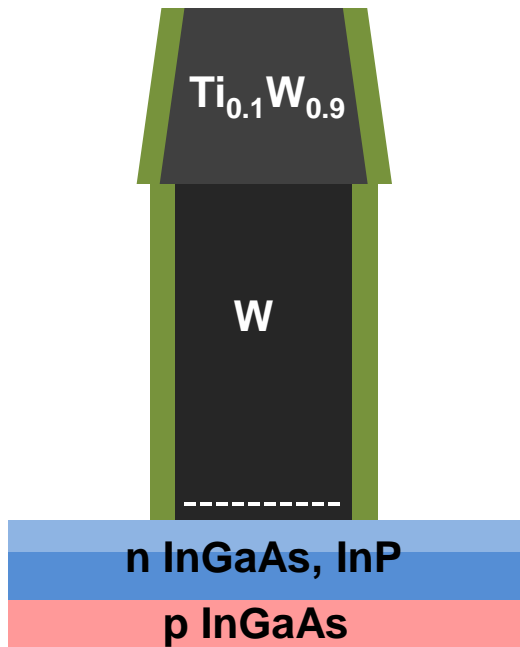


Fabrication: Emitter mesa

SiN_x PECVD deposition
CF₄/O₂ ICP etch

InGaAs wet etch

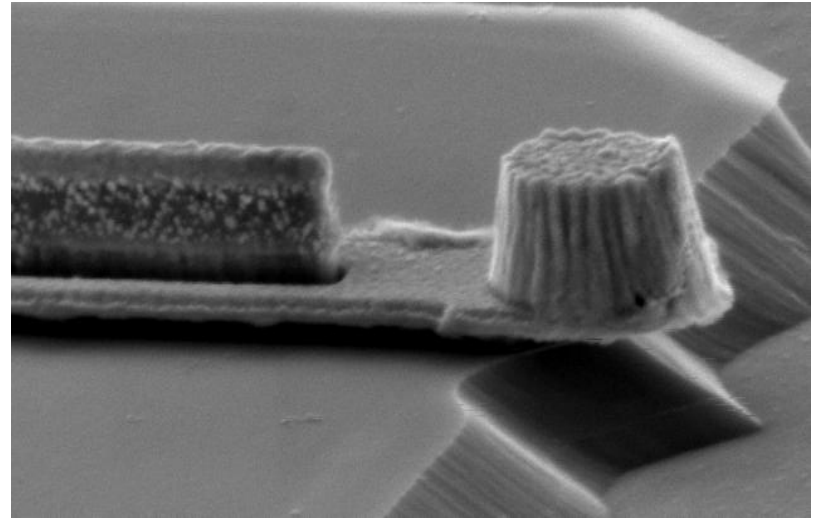
2nd SiN_x sidewall
InP wet etch



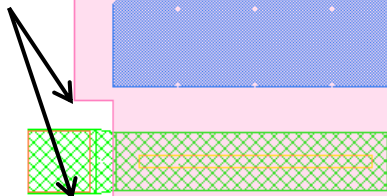
Base Post Cap

$$C_{cb,post} = \frac{\epsilon_0 \epsilon_r \cdot A_{post}}{T_c}$$

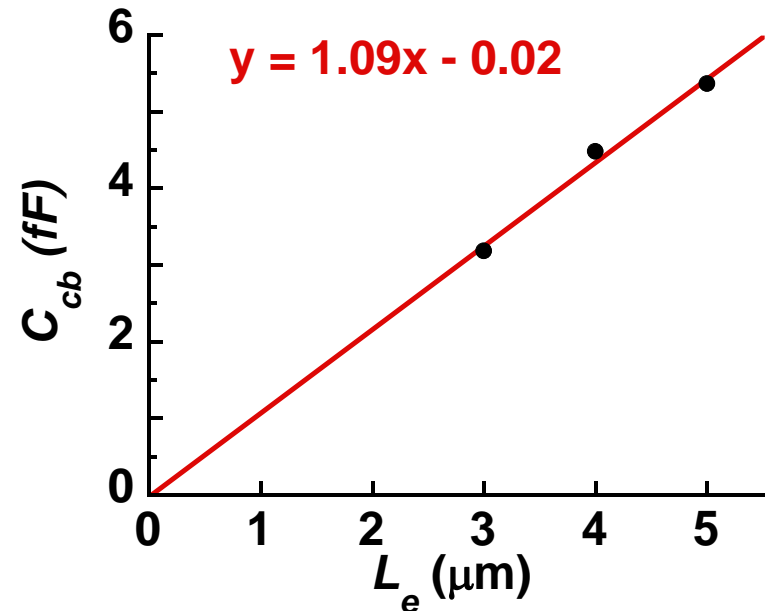
- $C_{cb,post}$ does not scale with L_e
→ Adversely effects f_{max} as $L_e \downarrow$
→ Need to minimize the $C_{cb,post}$ value

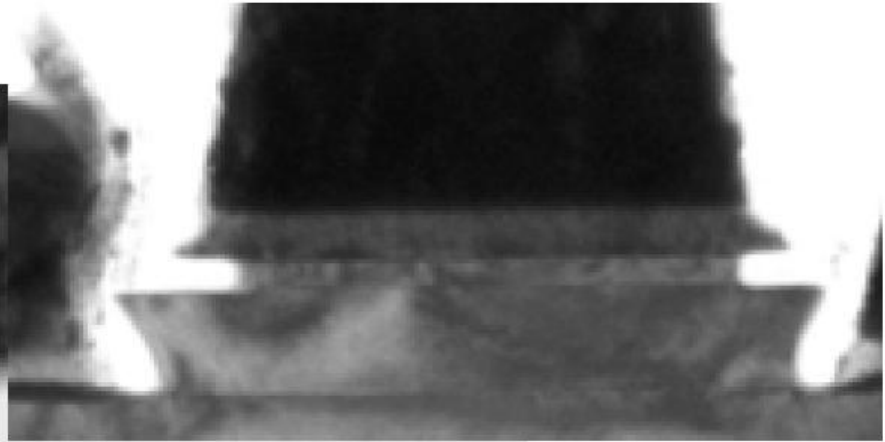
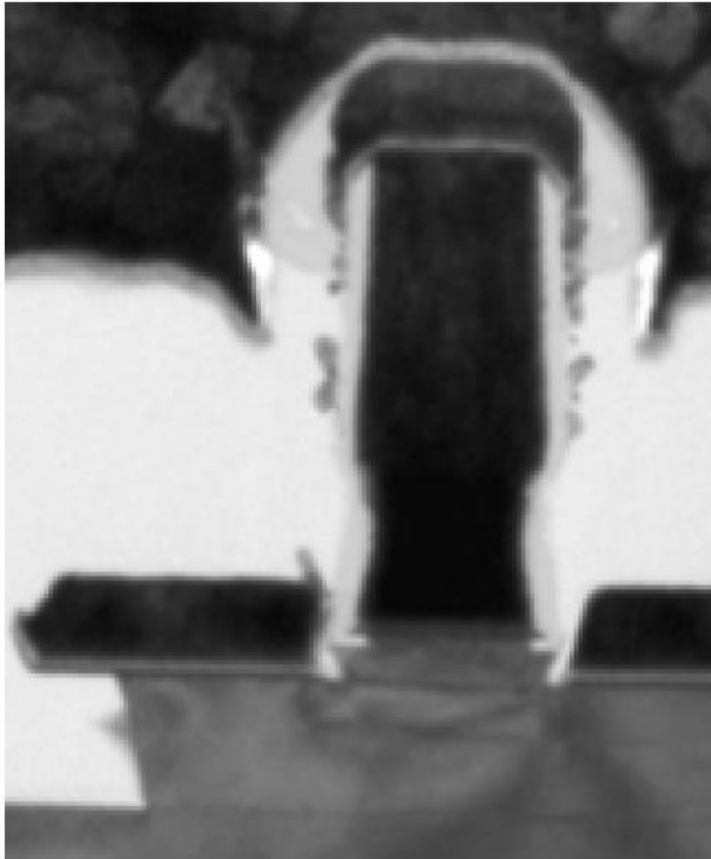


Undercut below base post



No contribution of Base post to C_{cb}





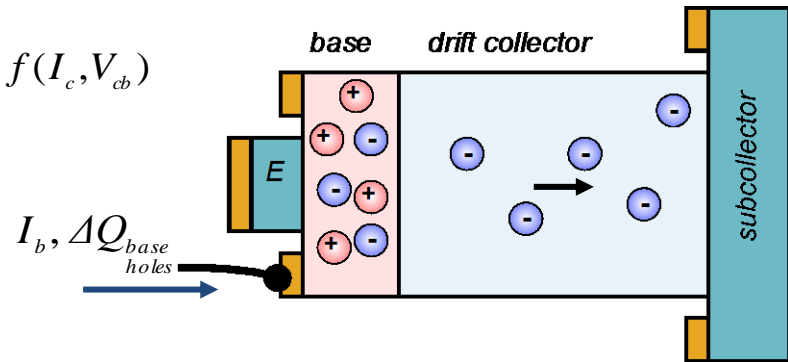
0.5 μm

Transit time Modulation Causes C_{cb} Modulation

$$Q_{base\ holes} = \text{constant} + Q_{base\ electrons} + \int_0^L qn(x)A(1-x/L)dx + V_{bc}\epsilon A/L = f(I_c, V_{cb})$$

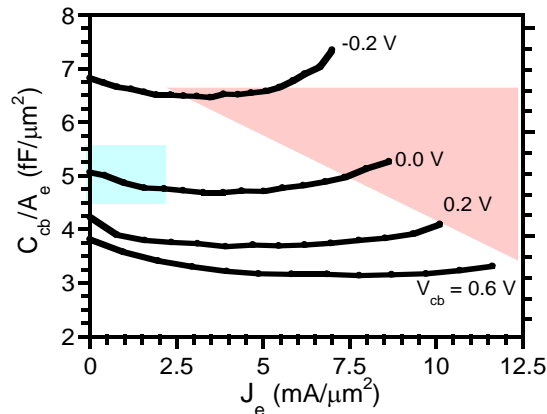
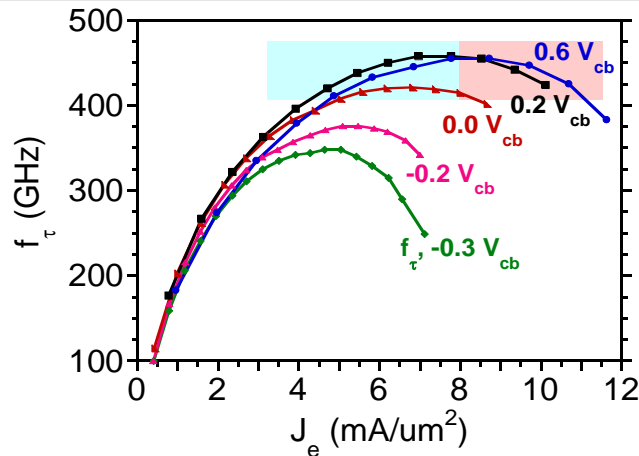
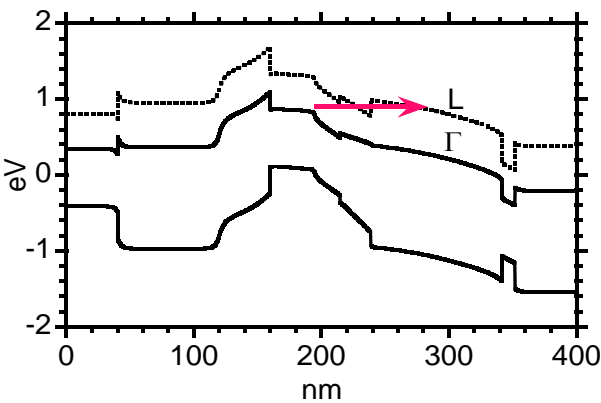
$$C_{cb} \equiv -\frac{\partial Q_{baseholes}}{\partial V_{cb}} \quad \tau_f \equiv \frac{\partial Q_{baseholes}}{\partial I_c} \Rightarrow \frac{\partial C_{cb}}{\partial I_c} = -\frac{\partial \tau_f}{\partial V_{cb}}$$

Carnitz and Moll, Betser & Ritter, D. Root



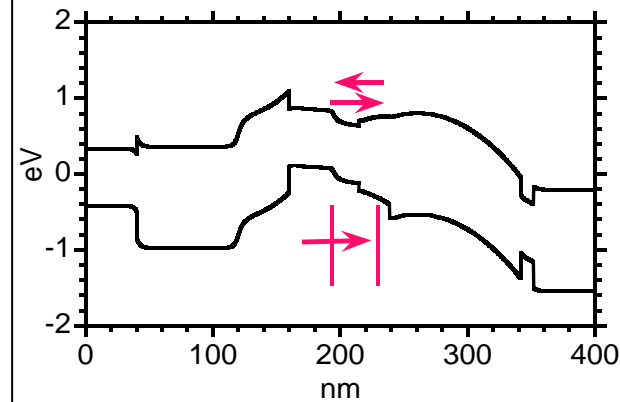
Collector Velocity Modulation:

$$\partial \tau_f / \partial V_{cb} > 0 \Rightarrow \partial C_{cb} / \partial I_c < 0$$



Kirk Effect:

$$\partial \tau_f / \partial V_{cb} < 0 \Rightarrow \partial C_{cb} / \partial I_c > 0$$



Increase in C_{cb} is due to both
 - base pushout into collector
 - and modulation of τ_b by V_{cb}

Increase in τ_c with $V_{cb} \rightarrow$ reduced C_{cb}

- strong effect in InGaAs SHBTs
- weak effect in InP DHBTs