

A 140GHz power amplifier with 20.5dBm output power and 20.8% PAE in 250-nm InP HBT technology

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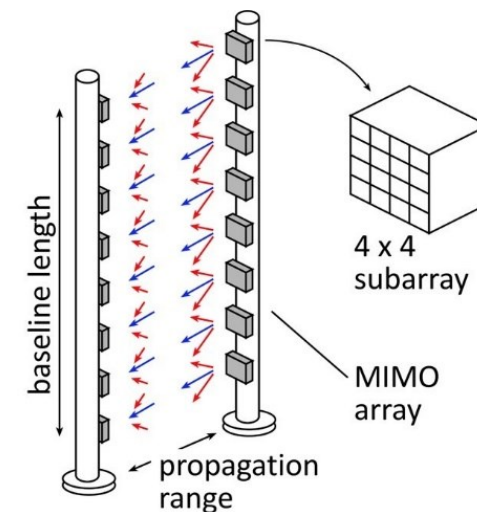
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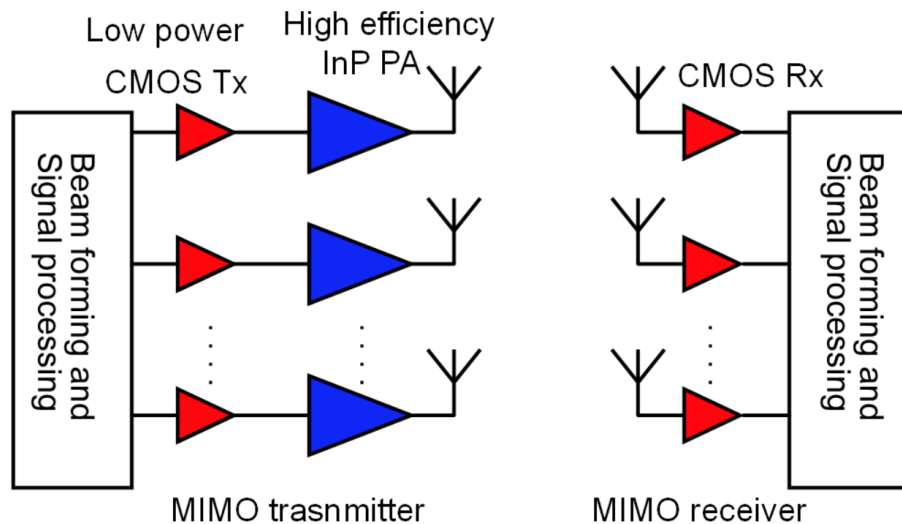
mm-wave Communication (140-1000 GHz)

- Objective
 - Support high data rate communication.
 - Spatial multiplexing for high capacity.
 - Cover long distance.
- Benefits (140- 1000 GHz)
 - Large available spectrum, high data rate.
 - Shorter λ : more channels for the same array size.
- Challenge
 - Atmospheric attenuation is high $P_R \propto \frac{\lambda^2}{R^2} e^{-\alpha R}$.



PA Requirments and Link Budget

- CMOS chips drives high efficiency InP power amplifiers
- CMOS's output power is ~2dBm
- 20.5dBm output power per element extends the link range to ~50m
- Required gain ~20dB
- Massive MIMO arrays requires high efficiency PAs to avoid thermal destruction or complex heatsink

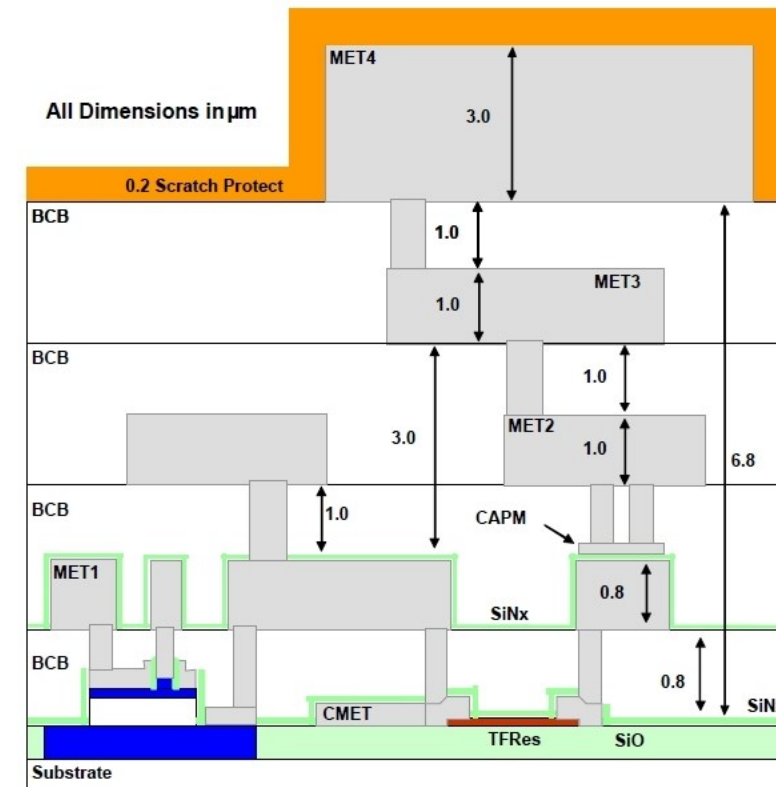
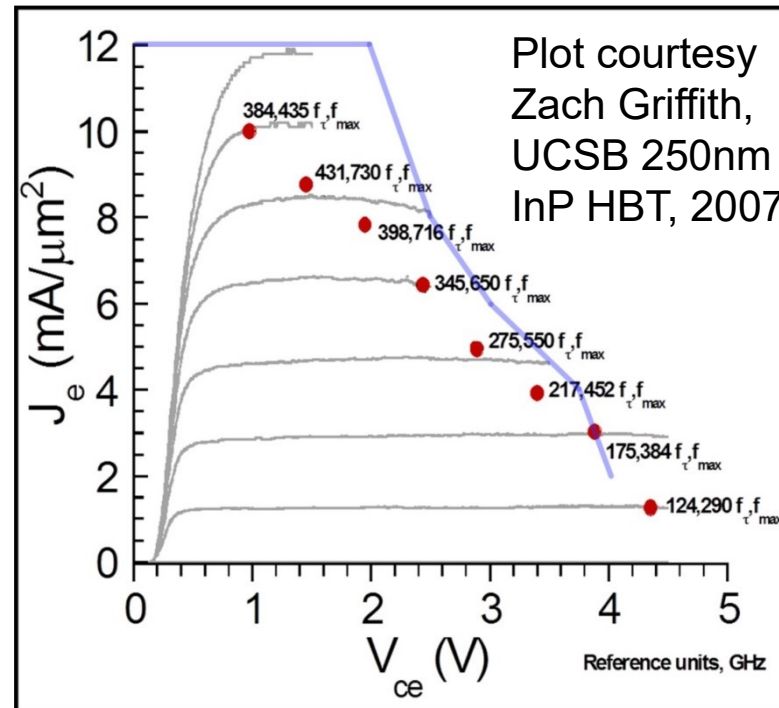


Tx Antenna Gain	22.7 dBi
Rx Antenna Gain	13 dBi
Link range	50 m
Required output power per element	20.5dB _m
Friss Path Loss	73 dB
Rx Noise Figure	8.5 dB
Rx BW	5 GHz
Bit rate	10 Gb/s
System Margin	15 dB
No of elements, Tx ($\lambda/2$ spacing)	32
No of elements, Rx ($\lambda/2$ spacing)	4

calculated data are based on <https://www.ece.ucsb.edu/Faculty/rodwell/Classes/ece218c/ECE218c.htm>

250nm InP HBT Process (Teledyne*)

- $f_{max} = 650\text{GHz}$.
- $BV_{CE0} = 4.5\text{V}$.
- $J_{max} = 3\text{mA}/\mu\text{m}$.
- Four Au interconnect.
- MIM cap ($0.3\text{fF}/\mu\text{m}^2$).
- TFR ($50\Omega/\text{square}$).

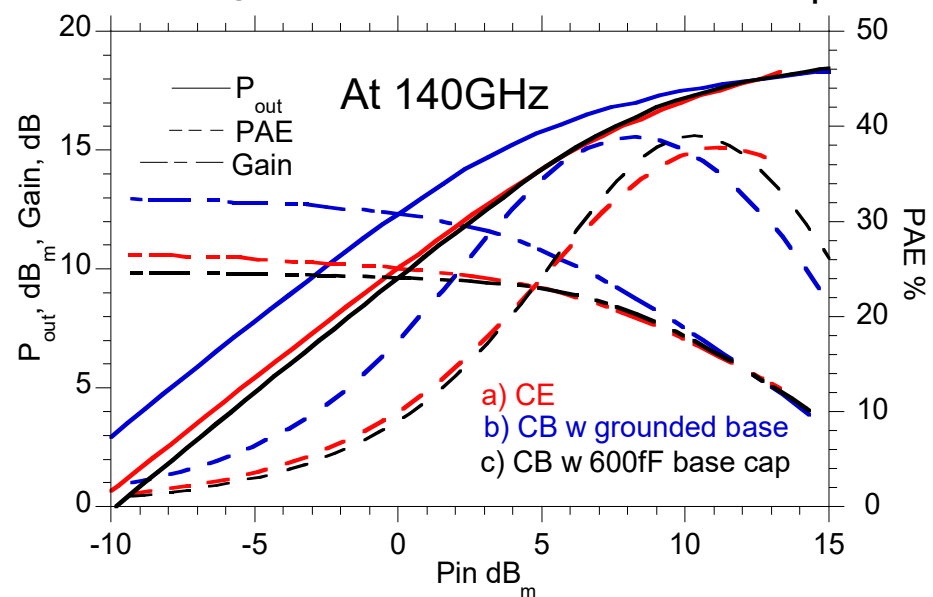
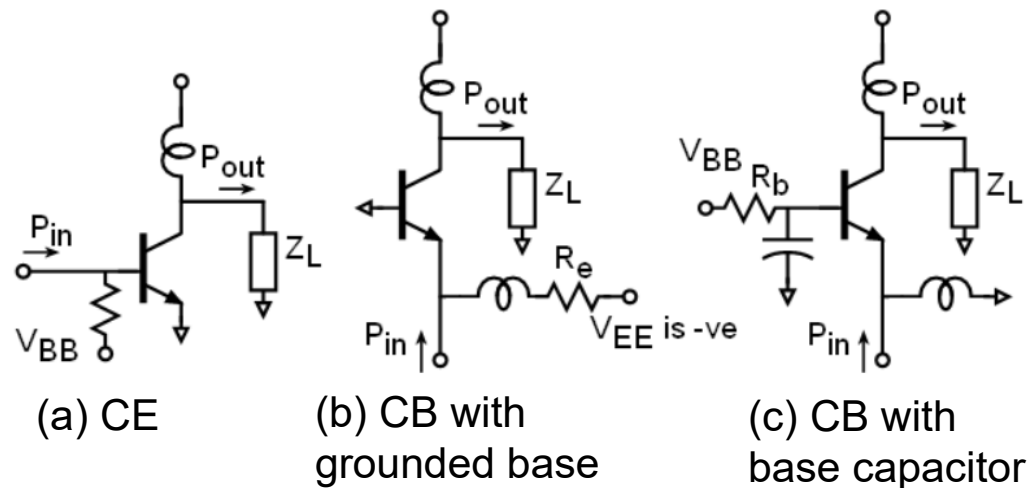


Representative cross-section of TSC250 IC technology. Drawing is not to scale.

*M. Urteaga, et al, Proc. IEEE, June 2017.

Unit Cell Comparison

- Comparison between CE, grounded CB and **CB with base capacitor**
- Simulation is done under same bias condition
- Large signal simulation is more relevant in power amplifier
- **CB with base capacitor shows the highest OP_{1dB} with associated PAE**



P_{out} , gain, and PAE for CE, grounded CB, and CB with base capacitor.

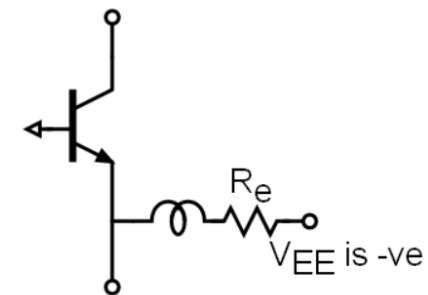
	Gain*, dB	PAE**, %	P_{out}^{**} , dB _m
CE	10.7	15.4	12.0
Grounded CB	13.1	22.4	13.5
CB with 600 cap	9.8	29.7	15.2

*under opt load line condition without compression **at 1dB gain compression

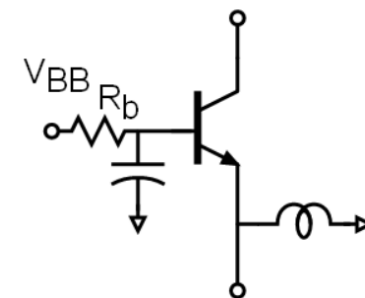
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- Common emitter
 - Lowest OP_{1dB} and Soft compression
 - Less sensitive to base inductance errors
- Common base with grounded base
 - Higher gain and OP_{1dB}
 - Requires –ve supply-> huge efficiency drop (large DC current in Re)
 - Bias is very sensitive without Re due to exponential relation (I_{CE} vs V_{BE})
 - sensitive to base inductance errors
- Common base with base capacitance
 - Highest PAE and OP_{1dB} due to capacitance feedback linearization
 - Capacitance help stabilization (not shown)
 - Stable bias: negligible efficiency due to R_b ; base current is very small
 - Gain drops with smaller capacitance



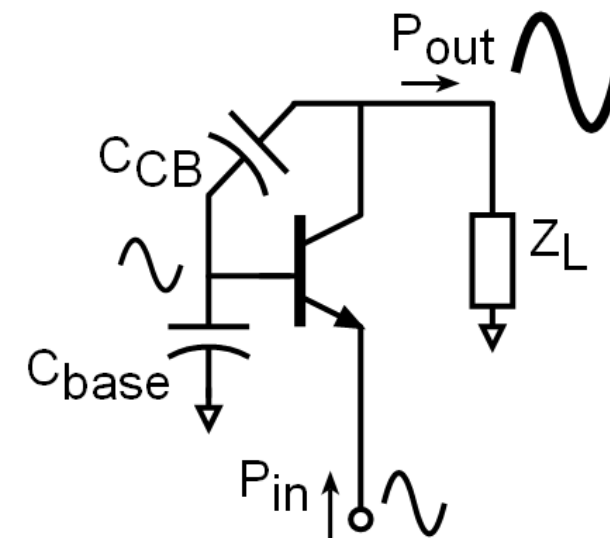
CB with grounded base



CB with base capacitor

CB viewed as stacked PA cell*

- C_{CB} and C_{base} creates negative feedback
- This negative feedback
 - Linearize the amplifier: higher PAE and OP_{1dB}
 - Allows voltage swing on the base:
with proper design, the output swing increases yielding in higher output power
 - Drops the output impedance: improves S22

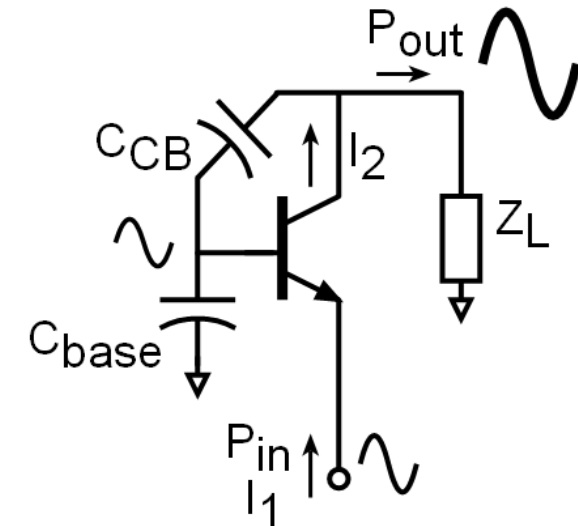


PA unit cell/ stack analogy

*A. Ahmed, et al, EUMIC 2018.

PAE invariance*

- Assuming lossless matching network
- Internal voltages and currents are constant by proper load and base impedances*
- $2(n - 1)\omega P_{add} C_{base} = X_1 X_2 \sin(Y_1 - Y_2)$
(derivation not shown)
- The added power per stage is kept constant for the same internal voltages and currents.
- $P_{out} = P_{add} + P_{in}$

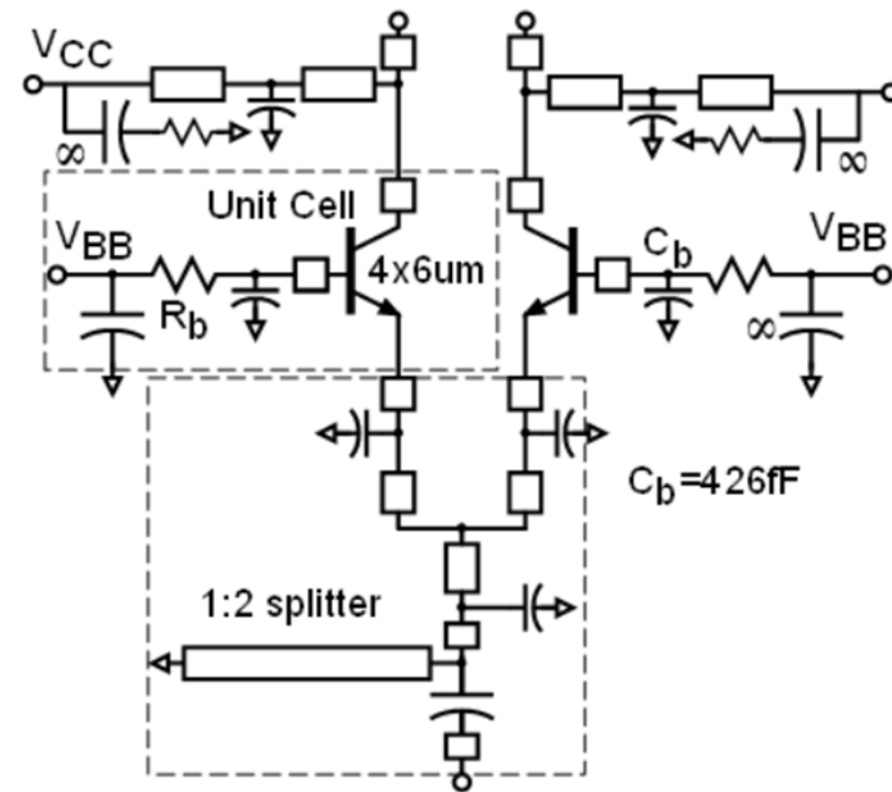


X_1 is the magnitude of I_1
 X_2 is the magnitude of I_2
 Y_1 is the angle of I_1 in radians
 Y_2 is the angle of I_2 in radians

*A. Ahmed, et al, EUMIC 2018.

Power Amplifier Cell

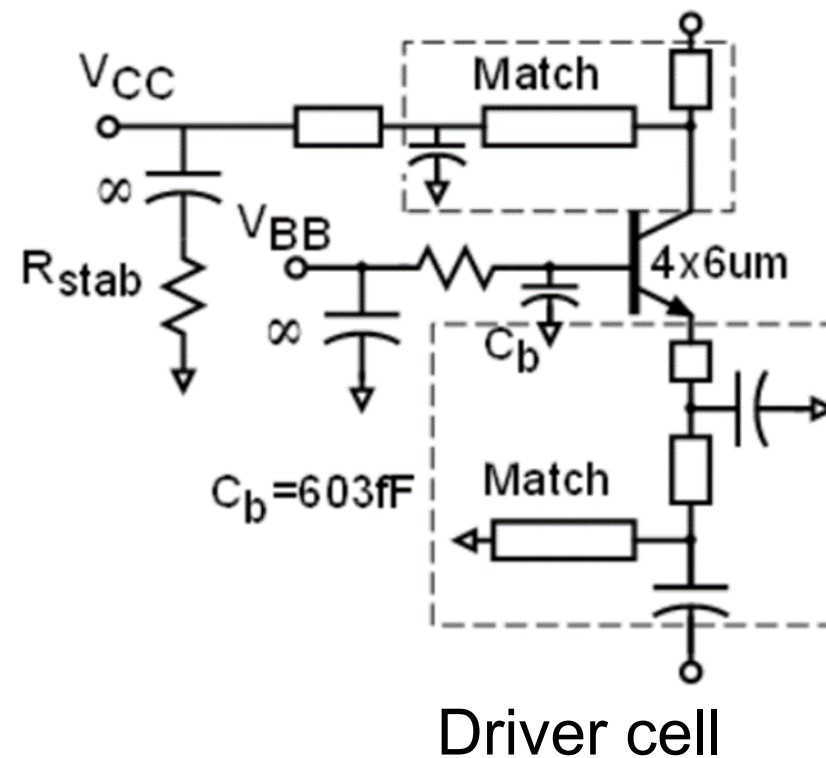
- Common base with base capacitance
- Capacitance dropped slightly
 - More power and hard compression
 - lower output impedance (better S22)
- Shunt stub tunes the transistor parasitics
- Two cells are combined and driven by a single driver-> better PAE
- ADS and HFSS are used for the interconnect and matching circuit simulations



Two combined PA cells

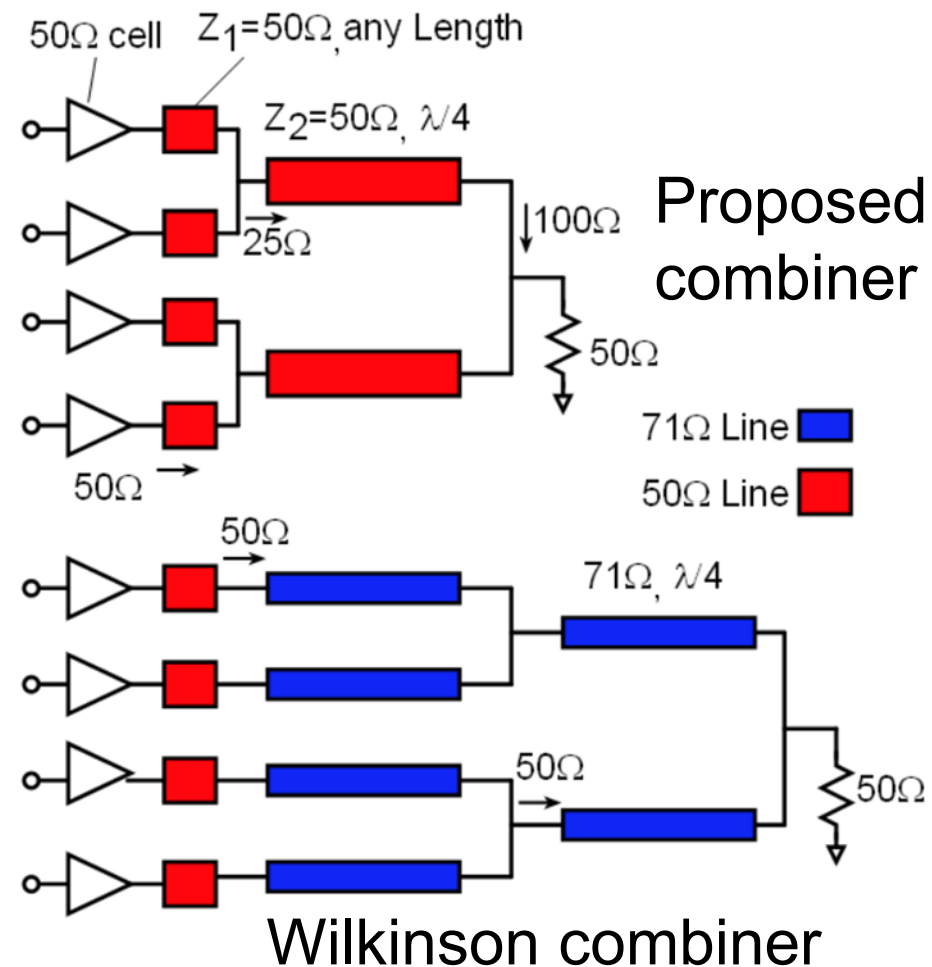
Driver design

- Higher base capacitance:
 - more gain
- Input ant output are 50Ω matched
- Staggered matching for wider bandwidth



Combiner Design

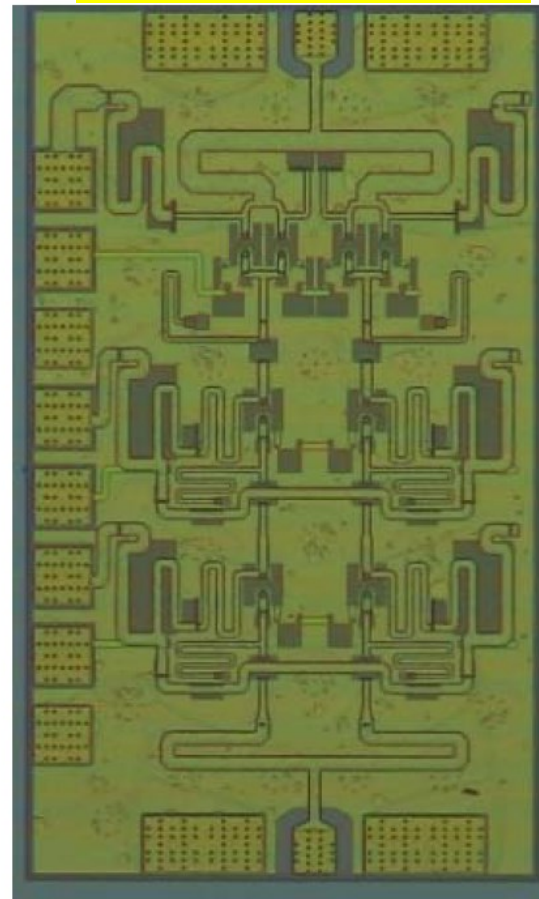
- Transmission line combiner instead of Wilkinson
- Proposed combiner
 - Low loss and very compact
 - Smaller BW compared to Wilkinson
- Wilkinson
 - Bulky, high loss and skinny line
 - Higher BW



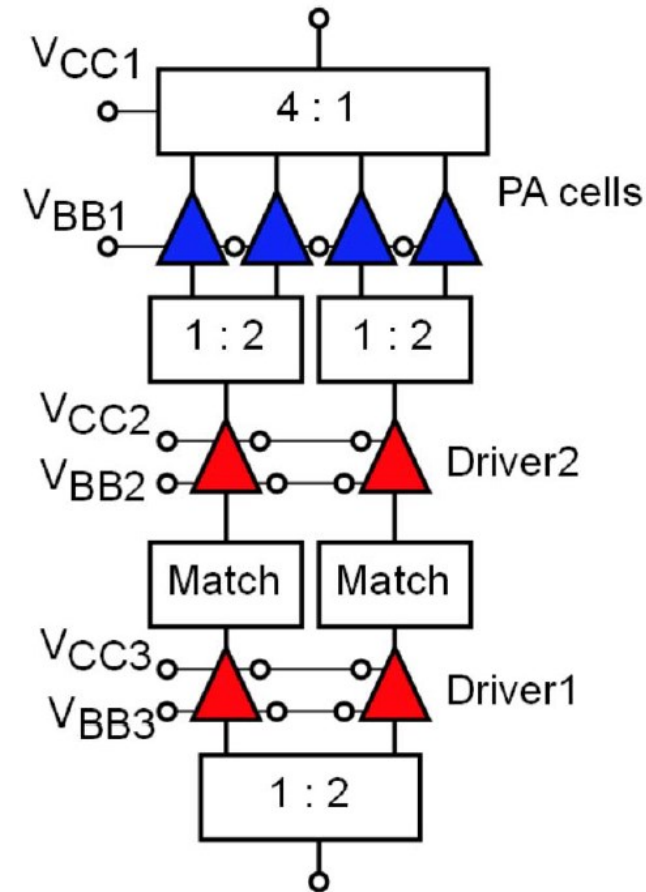
PA block diagram

1.08mmx0.63mm

- Three linearized common base stages
- Low loss and compact transmission line combiner
- First driver scaled to sustain good PAE
- Independent bias for each stage to monitor the current and optimize the PAE



Chip micrograph

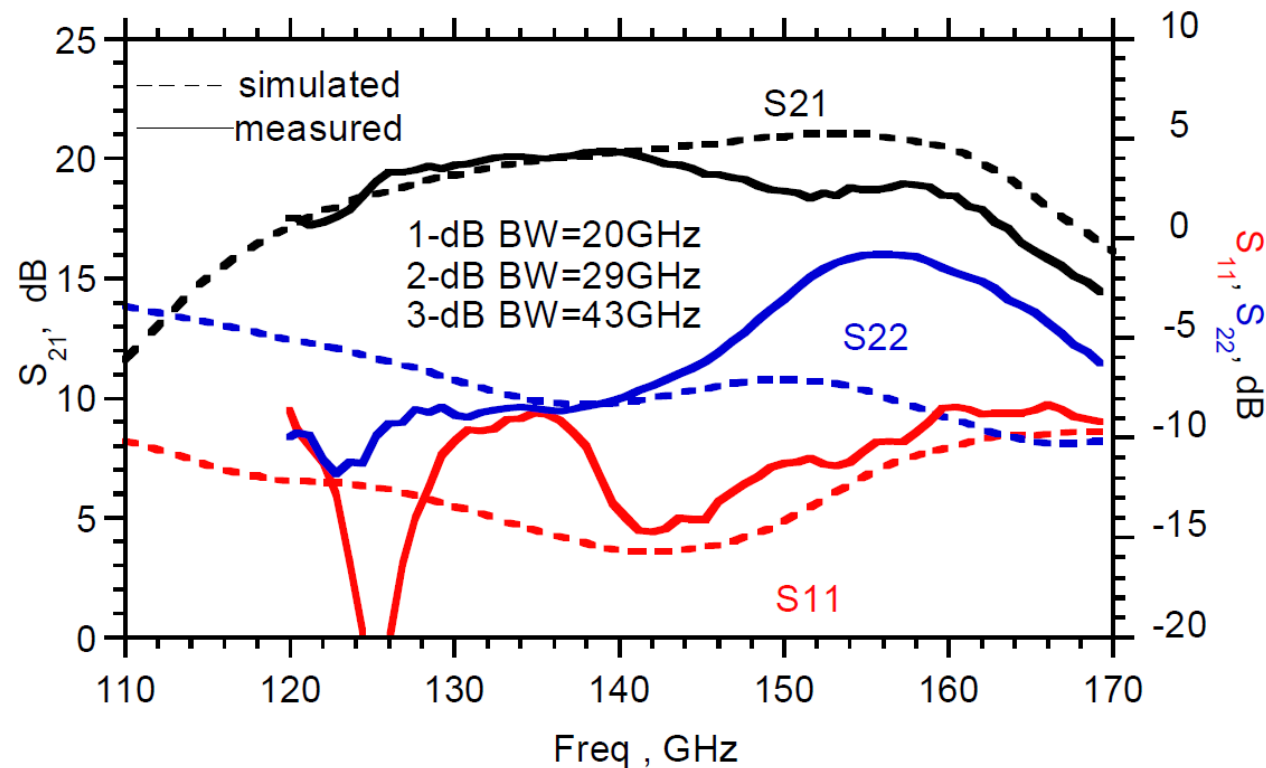


Block diagram

Measurement results

- Wide band operation
- 1dB BW=20GHz
- 3dB BW=43GHz

V_{CC1}	V_{CC2}	V_{CC3}	V_{BB1}	V_{BB2}	V_{BB3}
2.5V	2.5V	1.5V	1.94V	1.36V	1.1V
I_{CC1}	I_{CC2}	I_{CC3}	I_{BB1}	I_{BB2}	I_{BB3}
121mA	52mA	31.8mA	4.1mA	1.7mA	0.95mA

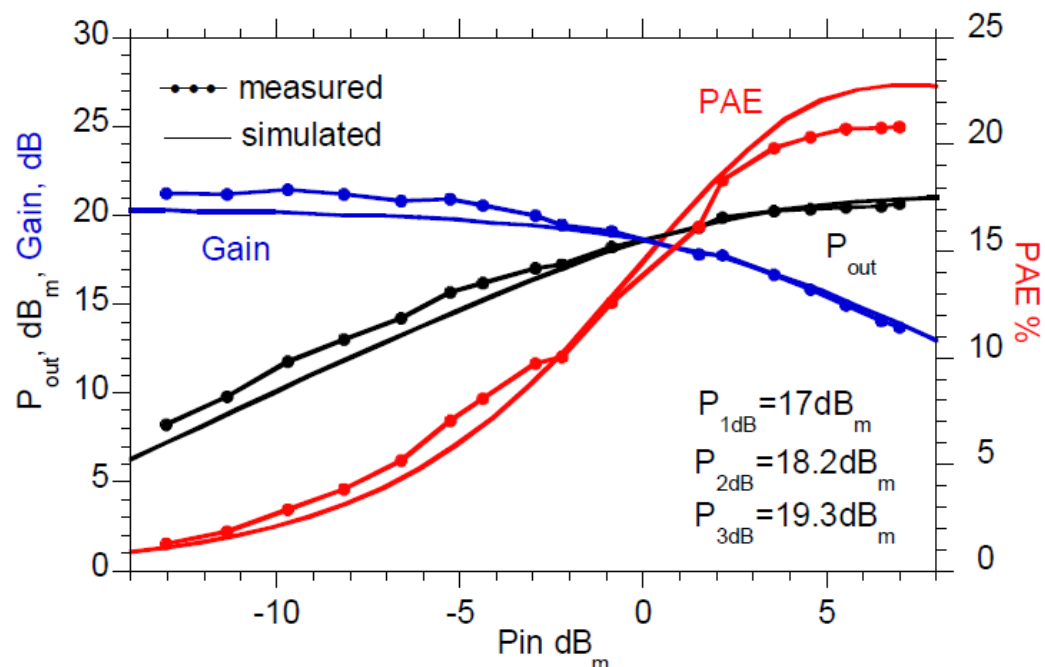


Measured (solid) vs simulated (dotted) S-parameters

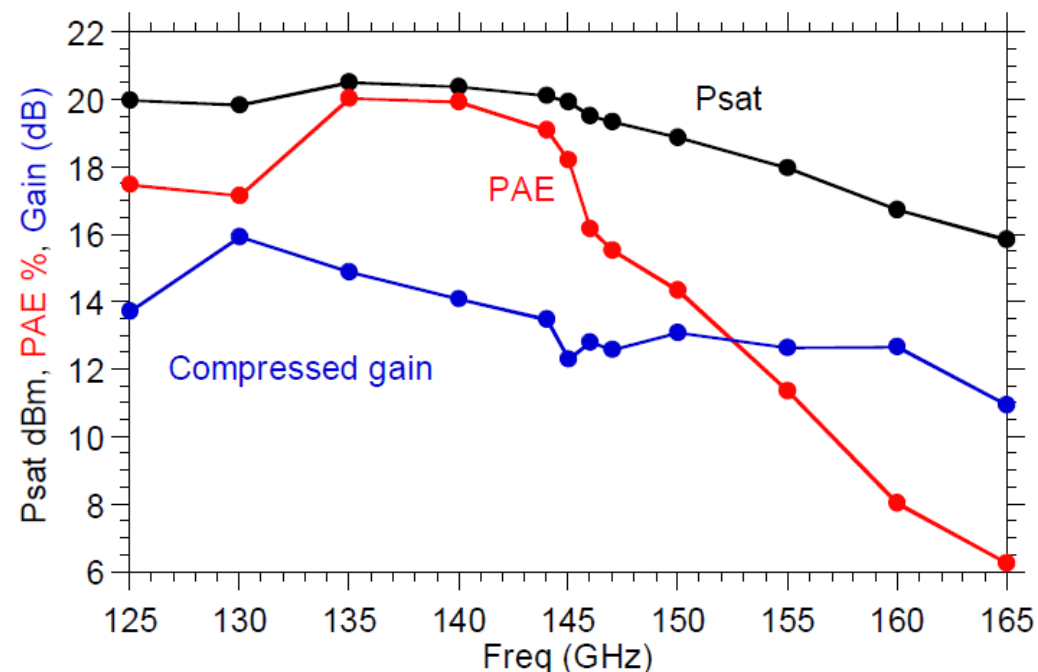
Measurement results

- $P_{sat} = 20.5 \text{ dB}_m$, and $\text{PAE} = 20.8\%$
- $P_{sat} = 18.9\text{-}20.5 \text{ dB}_m$ over 125-150GHz

V_{CC1}	V_{CC2}	V_{CC3}	V_{BB1}	V_{BB2}	V_{BB3}
2.5V	2.5V	1.5V	1.95V	1.4V	1.1V
I_{CC1}	I_{CC2}	I_{CC3}	I_{BB1}	I_{BB2}	I_{BB3}
130mA	56mA	34mA	5mA	2mA	1mA



Measured and simulated P_{out} , PAE and gain vs input power at 140GHz



Measured and simulated saturated P_{out} , PAE and gain vs frequency

State-of-the-art results

- Highest **PAE** for comparable P_{sat} and gain

Ref	Technology	Freq (GHz)	P_{sat} (dBm)	$BW_{3\text{dB}}$ GHz ⁺⁺	Gain at P_{sat} (dB)	Peak PAE %	Size (mm ²)	P_{DC} (W)	P_{sat} /Area mW/mm ²
[2]	40 nm CMOS	140	14.8	17	13**	8.9	0.34	0.3	88.8
[4]	130-nm SiGe HBT	155-180	18.0	25	23.5**	4.0	0.85	1.57*	74.2
[5]	130-nm SiGe HBT	112-142	17 ⁺	16	29**	13 ⁺	1.06	0.39*	47.2
[6]	130-nm SiGe HBT	131-180	14	49	22**	5.7	0.48	0.44*	52.3
[7]	250-nm InP HBT	110-150	23.2-24.0	32.7	14-16	5.8-7.0	1.89	3.46	134
[8]	250-nm InP HBT	115-150	21-21.8	34.8	15-17.5	8.2-10.5	0.75	1.54	205
This work	250-nm InP HBT	125-150	18.9-20.5	43	12.3-15.9	14.3-20.8	0.69	0.52	162

Summary

- Demonstration of record PAE at D-band
- Teledyne 250nm InP HBT has high f_{\max} and BV_{CE0}
- Capacitively linearized common base
 - Higher OP_{1dB} , and PAE
 - Easier to bias and stabilize
- Compact and low loss transmission line network
- Driver scaling and bias optimization

Acknowledgement

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