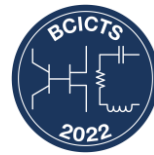




Paper 2b.2



A 280 GHz (x8) Frequency Multiplier Chain in 250 nm InP HBT Technology

Utku Soylu¹

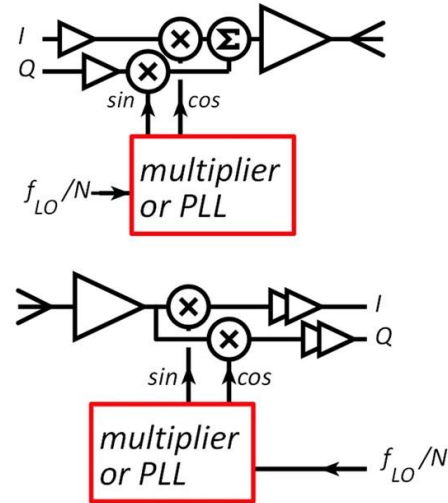
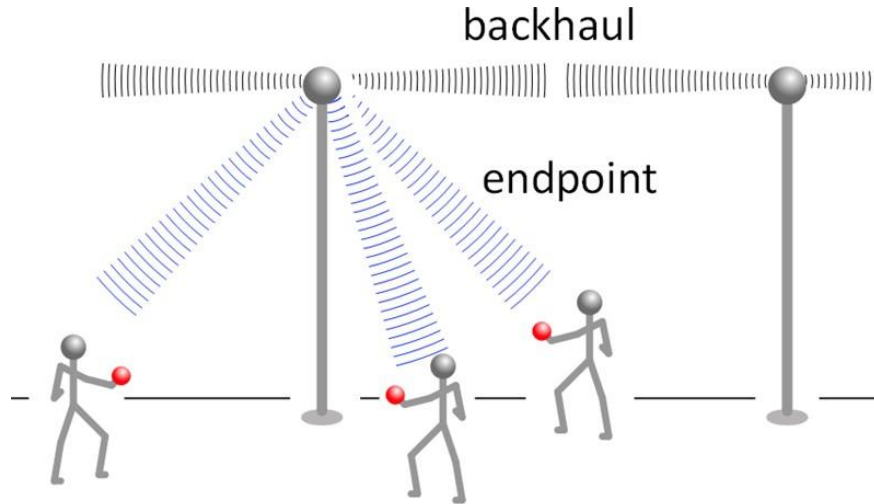
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200-300 GHz Wireless Backhaul

Growing demand for wireless communications: endpoint and backhaul
 200-300 GHz backhaul: 100+ Gb/s feasible over $\sim$ km range.
 → develop 200-300 GHz transceivers



mm-wave LO generation

PLLs:

in-band phase noise: $N^2 \times \text{reference}$ (plus additive noise)

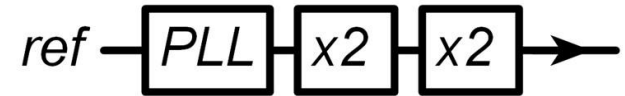
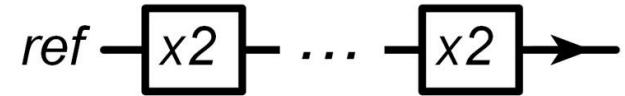
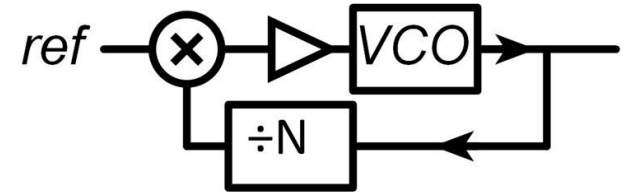
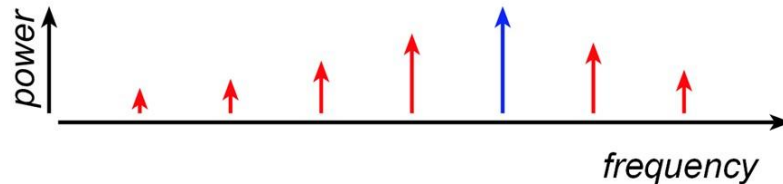
out-of-band phase noise: VCO

challenge: low-noise mm-wave VCO

Multipliers:

phase noise: $N^2 \times \text{reference}$ (plus additive noise)

spurious harmonics: out-of-band response

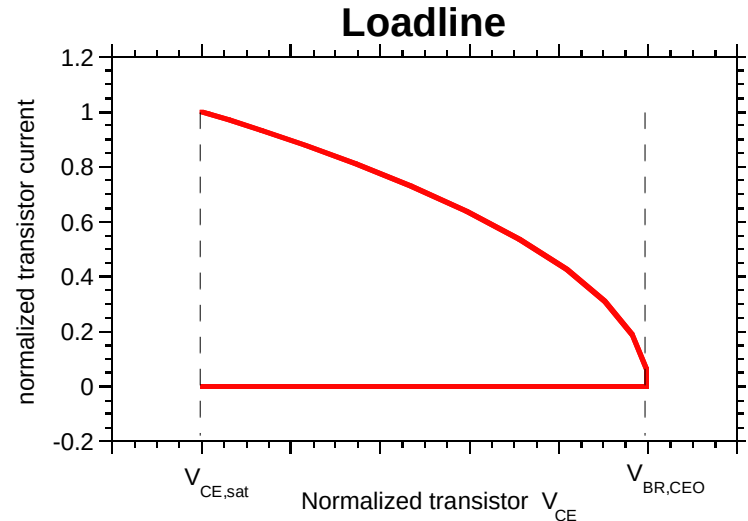
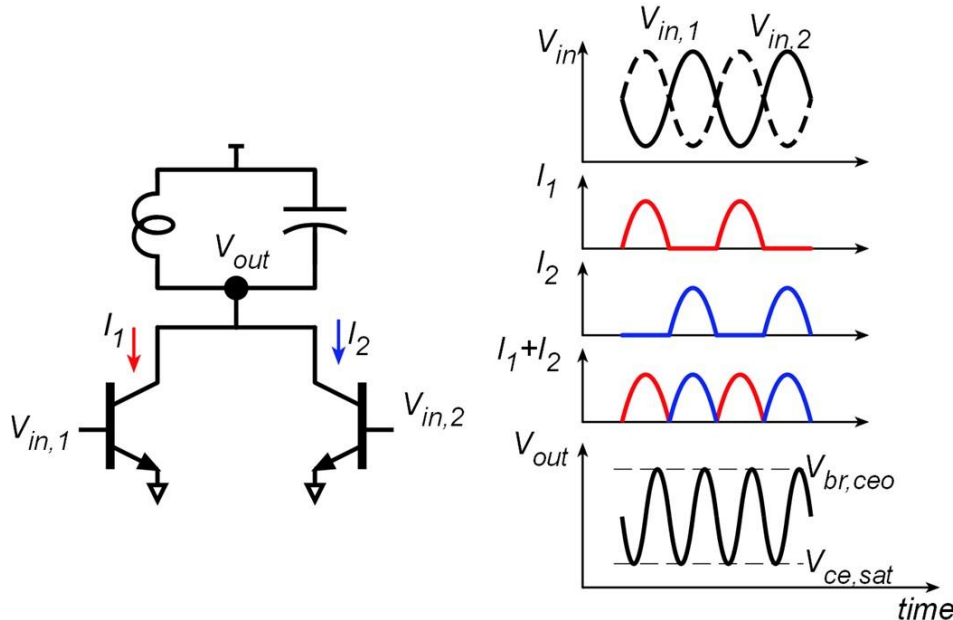


Push-Push Frequency Doubler

Push-push: odd harmonic suppression.

Maximum P_{out} design: voltage swing between $V_{ce,sat}$ and $V_{br,ceo}$.

Here: loadline instead tuned for maximum PAE (smaller V_{max}).

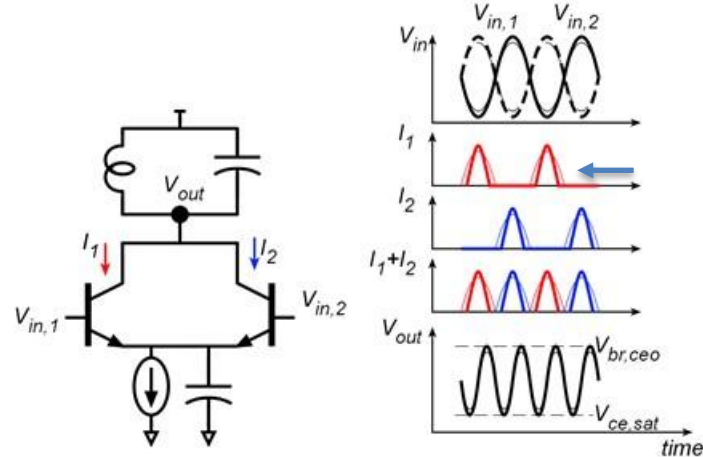
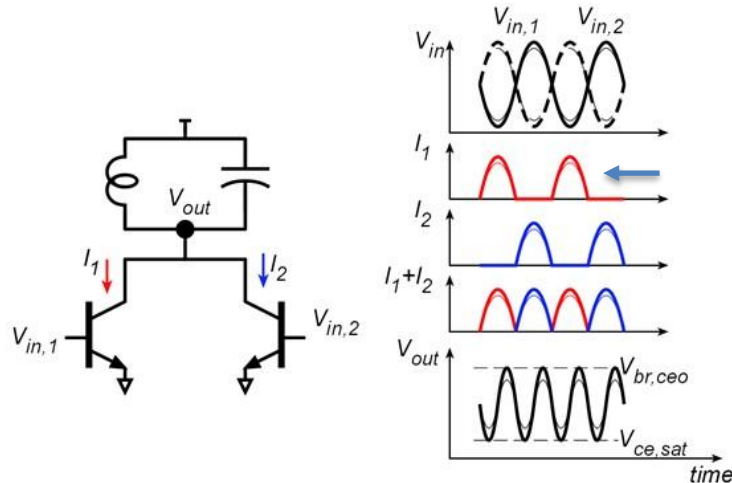
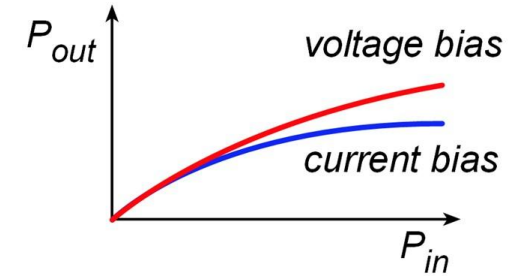


Doubler: Voltage vs. Current Bias

Voltage bias: output current & charge increase with P_{in} .

Current bias: output charge independent of P_{in} .

→ less variation of P_{out} with P_{in} .



Teledyne 250 nm InP HBT

$$f_{\max} = 650 \text{ GHz.}$$

$$J_{\max} = 3 \text{ mA}/\mu\text{m.}$$

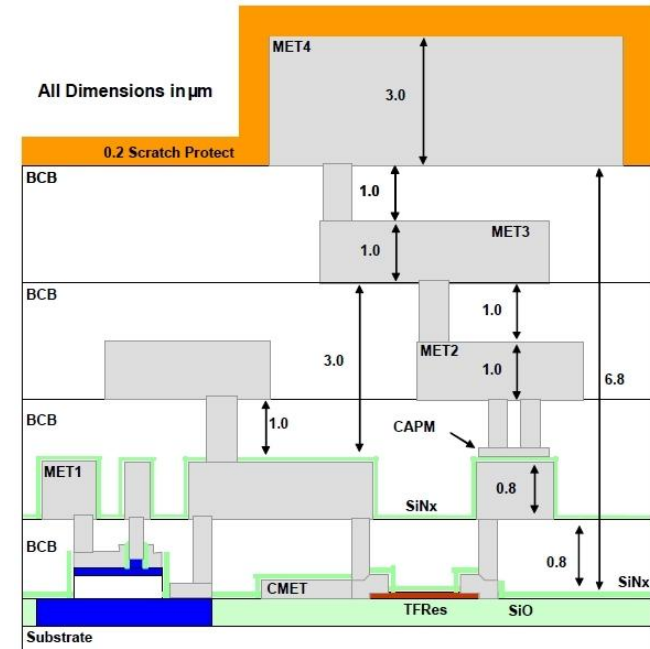
$$B_{VCE0} = 4.5 \text{ V.}$$

Four interconnect levels

Microstrip lines (M4 signal, M1 ground)
1.0 dB/mm @ 280 GHz

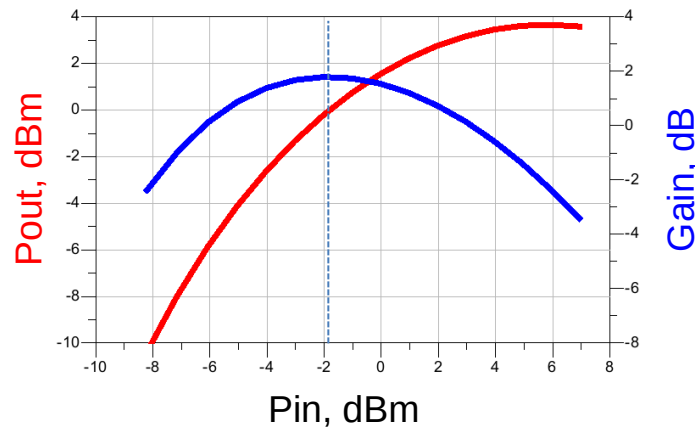
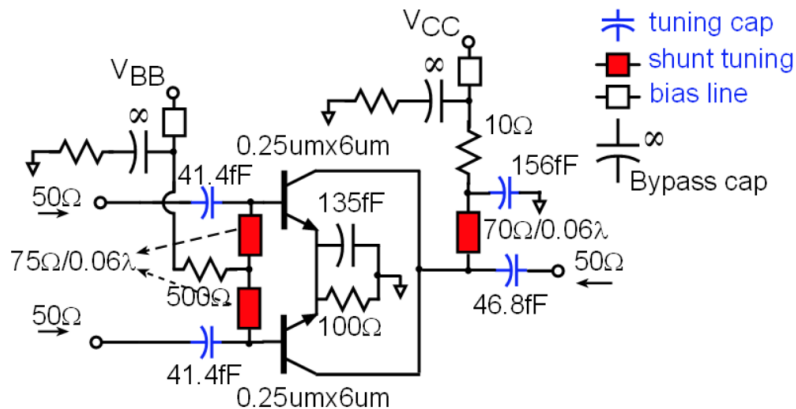
Resistors: 50 Ω /square

MIM capacitors: 0.3 fF/ μm^2



Representative cross-section of TSC250 IC technology. Drawing is not to scale.

Doubler Area Scaling/Bias Condition



HBT emitter length set such that $P_{out} > P_{in}$.

→ Cascaded doublers don't need inter-stage amplifiers .

Input/Output Matching

140 GHz input tuning: 50 Ω large-signal match

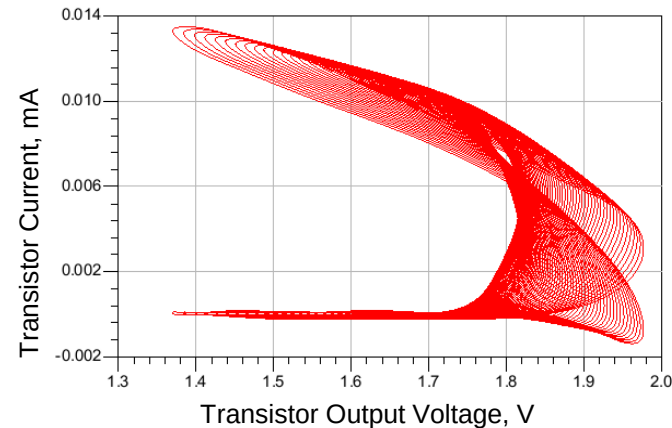
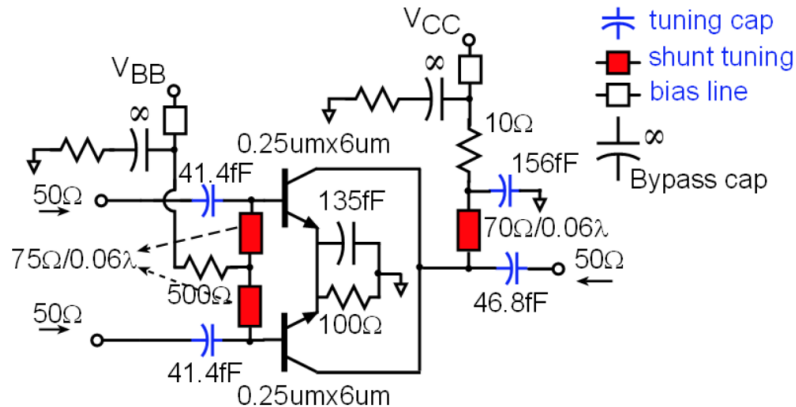
280 GHz output (50 Ω load):

current swing at HBT safe limits (2.3 mA/ μ m)

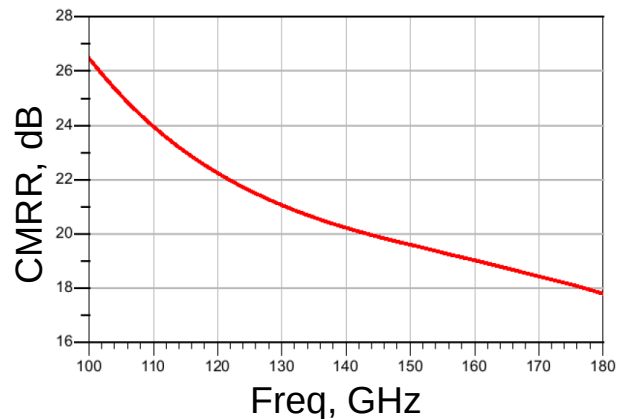
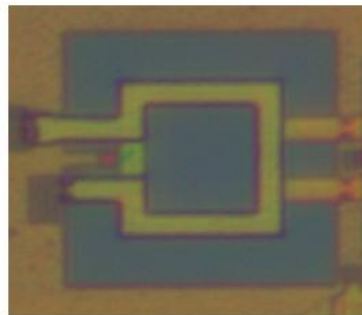
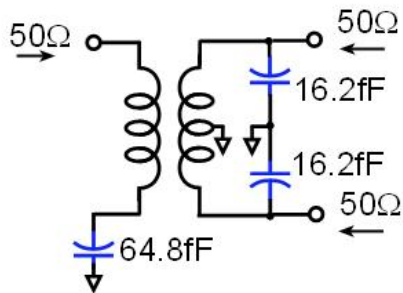
voltage swing below HBT ($V_{BRCEO} - V_{CE,sat}$) limits:

less saturated output power but greater gain.

Emitter RC network improves low-frequency common-mode stability.



Single-ended to Differential Conversion

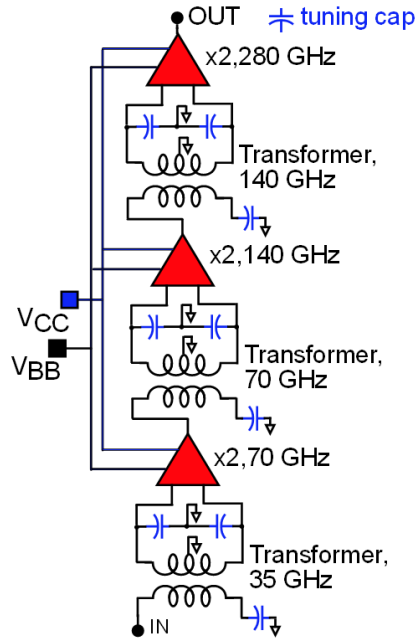
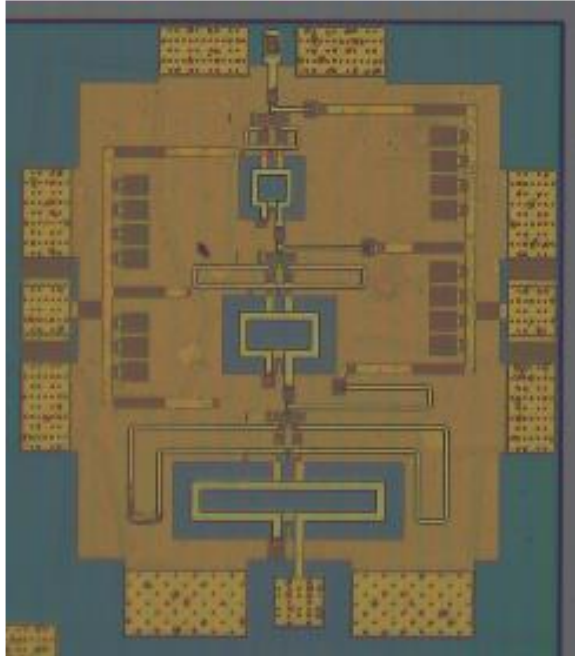


0.5 dB loss at 140 GHz.

Simulated phase imbalance: 10° & Simulated amplitude imbalance: 0.2 dB

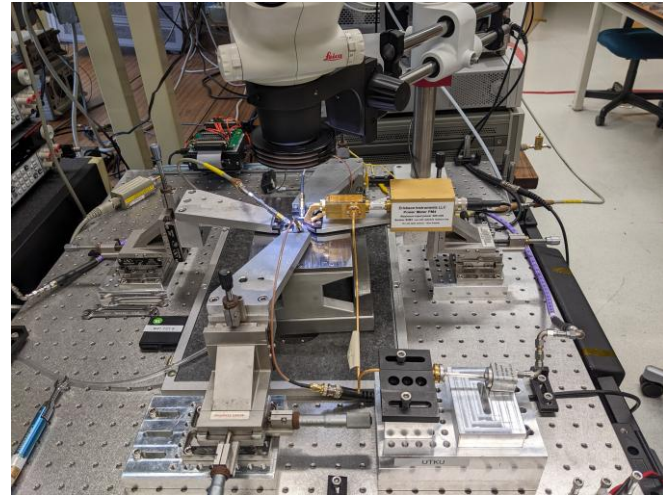
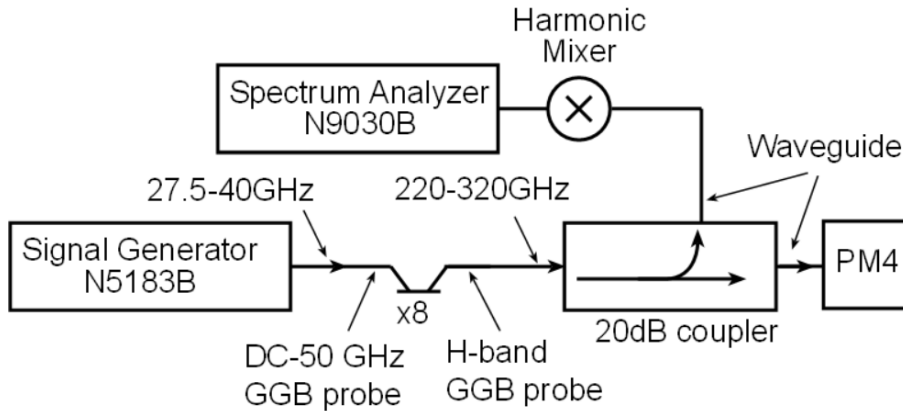
Single-ended input to differential output amplifier with high CMRR:
Better spurious harmonic rejection at the expense of DC power consumption.

x8 Frequency Multiplier Chain



280GHz Pin = -2 dBm	0.25um x 6um, 3 cascaded x2
Multiplication	x8
BW_{3dB}	48 GHz
P_{out}	-0.6 dBm
P_{DC}	112 mW
Die Area	0.4 mm ²
Spurious Harmonic Suppression	28 dBc

Power Measurement Setup

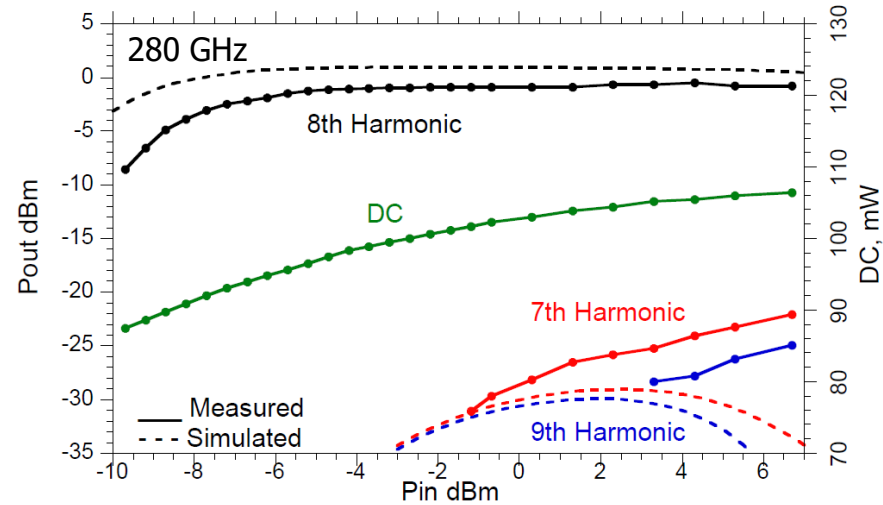


Simultaneous power and spectrum measurement.

Spurious-free tone to calculate cross-calibration coefficient generated by FMC.

High-order passive harmonic mixer limits minimum detectable signal power.

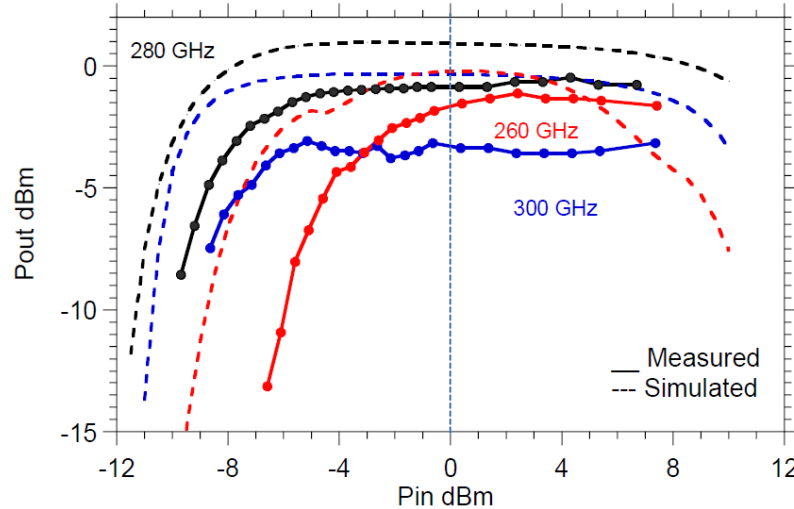
Measurement Results: P_{out} vs P_{in}



$$P_{in} = -1.2 \text{ dBm} \rightarrow P_{out(@7th \text{ harmonic})} = -31 \text{ dBm}$$

$$P_{in} = 3.3 \text{ dBm} \rightarrow P_{out(@9th \text{ harmonic})} = -28.3 \text{ dBm}$$

Measurement Results: P_{out} vs P_{in}



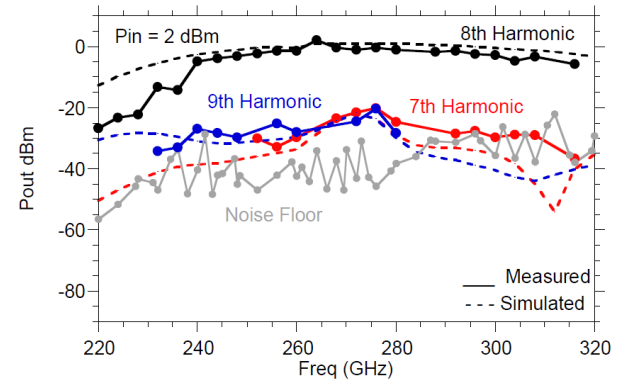
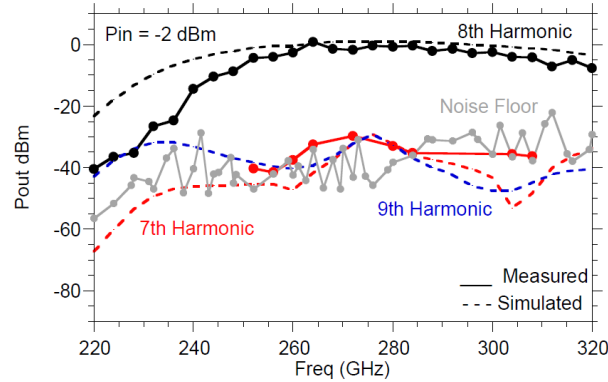
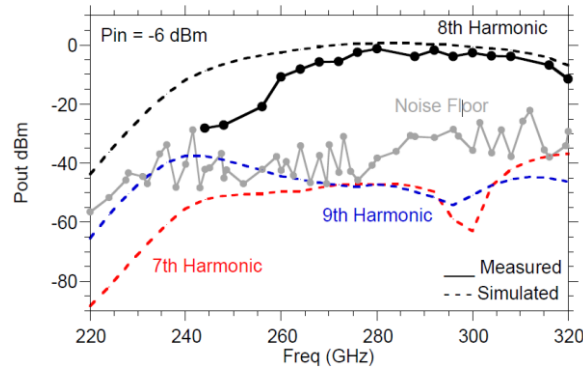
P_{in} = 0 dBm:

280 GHz: Measured P_{out} : **-0.8 dBm**, Simulated P_{out} : 0.9 dBm

300 GHz: Measured P_{out} : **-3.3 dBm**, Simulated P_{out} : -0.3 dBm

Inaccurate large-signal device modelling at high frequencies.

Measurement Results: Pout vs freq



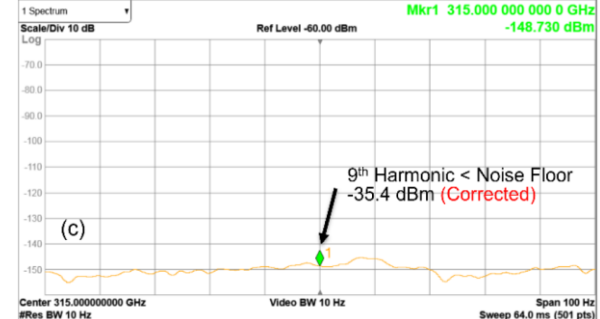
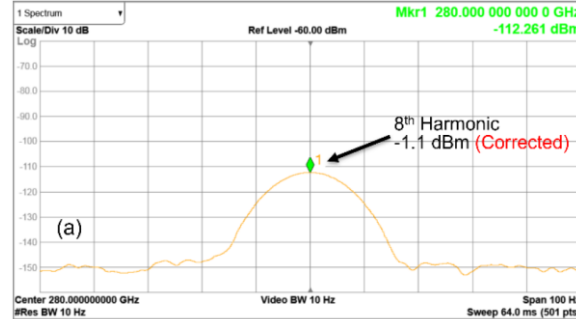
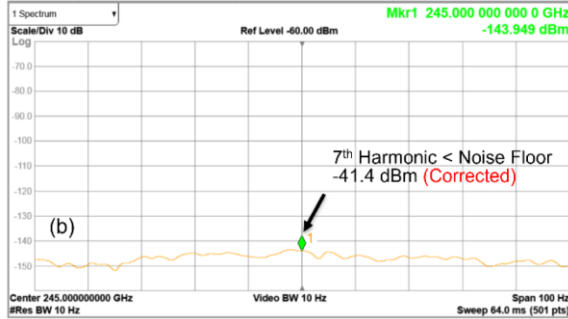
$P_{in} = -2 \text{ dBm} \rightarrow 2 \text{ dBm}$:

3-dB bandwidth: 48 GHz $\rightarrow$ 60 GHz.

Harmonic suppression: 28 dBc $\rightarrow$ 20 dBc

Set P_{in} for high spectral purity or wider operating bandwidth.

Measurement Results: Output Spectrum

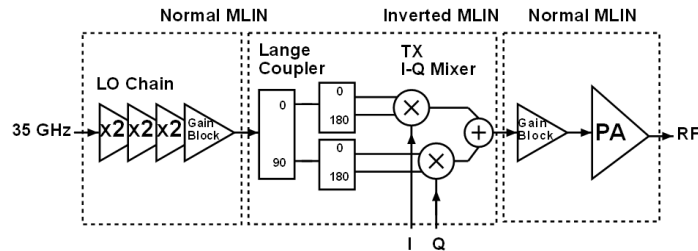
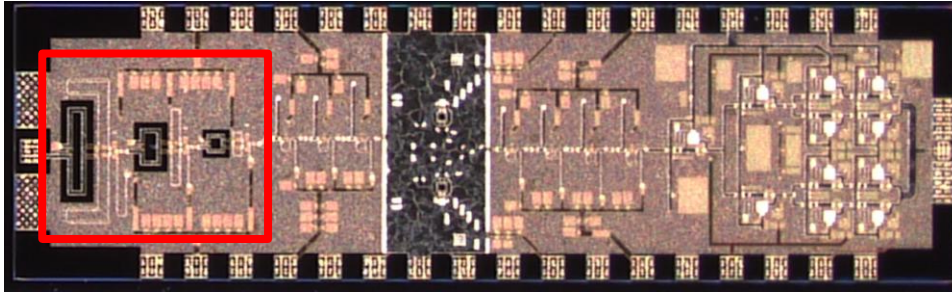


$P_{in} = -6$ dBm: Spurious harmonics are below the noise floor.

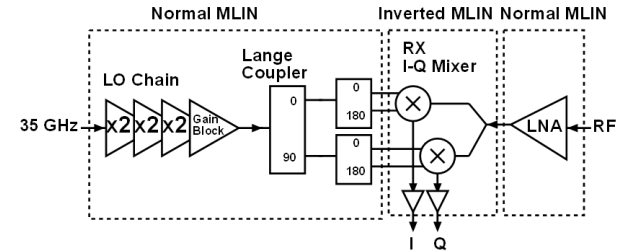
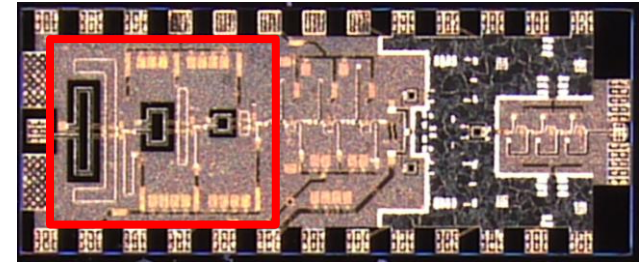
Low order/fundamental mixer → better dynamic range.

Transmitter/Receiver with x8 FMC

280 GHz direct-conversion TX



280 GHz direct-conversion RX



Performance Comparison

Table 1. State-of-the-art H-band frequency multipliers.

Ref	[2]	[3]	[4]	[5]	[6]	[7]	[8]	[9]	[10]	This work
Freq, GHz	240	159	244.5	260	252	250	255	300	300	280
Multiplication	x18	x6	x8	x8	x4	x6	x16	x3	x8	x8
BW _{3dB} , GHz	41	48 ^c	81	100	48	45	40	22	127	48
P_{out} , dBm	6.2	4.6	-7.7	2.5	5.5	5	-6	2.3	2.3	-0.6
P_{DC} , mW	429	100	240	-	270	124.8	300	410	537	112
Chip Size, mm ²	0.28	0.25	0.86	3.25	0.29 ^d	2 ^d	0.7	1.85 ^d	1 ^d	0.4
Spurious Harmonic Suppression, dBc	25	13	28	< 10 ^a	20	-	30 ^b	-	16 ^b	28
Technology	130-nm SiGe BiCMOS	250-nm InP HBT	130-nm SiGe BiCMOS	GaAs mHEMT	130-nm SiGe BiCMOS	InP HEMT	130-nm SiGe BiCMOS	40 nm CMOS	130-nm SiGe BiCMOS	250-nm InP HBT

^agraphically estimated, ^bsimulated, ^cBW_{3dB}, ^dincluding pads

This work shows **record spectral purity** among H-band frequency multipliers.

Acknowledgement

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THANK YOU

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Power Measurement Setup (Pictures)

